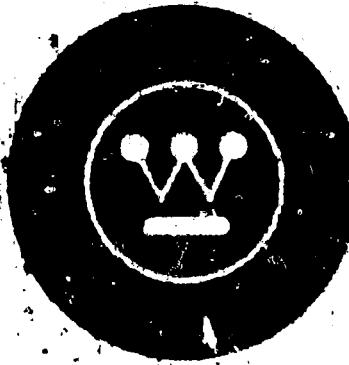


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WANL-TME-1710  
November, 1967



**Westinghouse Astronuclear Laboratory**

NUCLEAR HEATING MEASUREMENT

IN THE PLUM BROOK REACTOR (RE-4)

**MASTER**



Astronuclear  
Laboratory  
WANL-TME-1710  
November, 1967

NUCLEAR HEATING MEASUREMENT  
IN THE PLUM BROOK REACTOR (RE-4)

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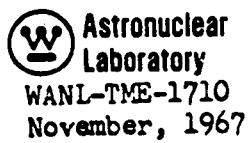
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#### ABSTRACT

An aluminum pedestal type calorimeter was used to measure nuclear heat generation rates in HT-1 (Horizontal Through Hole No. 1) of the Plum Brook Reactor Facility. The nuclear heating rate on the HT-1 axis at the core North-South vertical midplane averaged 3.73 watts/gm over the eight days that it was measured with a maximum of 3.78 watts/gm, when the reactor control rod bank position was near 23 inches. The nuclear heating measurement at this location is shown to be accurate to  $\pm 7.5\%$  at the 95% confidence level.

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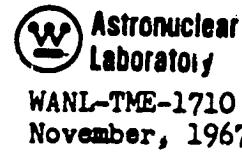


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## 1.0 INTRODUCTION

Materials and instrument transducers are to be irradiated at cryogenic temperatures in a test capsule (Figure 1) in the Plum Brook Reactor Facility in support of the NERVA (Nuclear Engine for Rocket Vehicle Application) program. It is important to duplicate, with a high level of confidence, both the fast neutron flux and the nuclear radiation heating that these transducers experience in NERVA environments. The current prediction of radiation heating in this test region is accurate to  $\pm 2\%$  at the 95% confidence limit (Reference 10). A knowledge of the radiation heating should be more accurate than this to provide the optimum relationship between test program and definition of limits for application. These measurements make use of aluminum cylindrical calorimeters; the basic design was previously used successfully (References 1-3).

The calorimeter shown in Figure 2 consisting of three aluminum cylinders was used to measure nuclear heating rates on nine different days in the 65-P cycle along the HT-1 axis and along the line perpendicular to the core vertical surface intersecting the HT-1 axis as shown in Figure 1.



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## 2.0 SUMMARY

Average values of nuclear heating rate at the core North-South vertical midplane are 4.94, 3.73, and 3.12 watts/gm for the near, middle, and far calorimeter cylinders, respectively at 60 MW reactor power. The middle cylinder is on the HT-1 axis, while the near and far cylinders are 2.5 inches toward and away from the core, respectively. Maximum values of the above heating rates at 60 MW are 5.00, 3.78, and 3.15 watts/gm for the near, middle, and far calorimeter cylinders, respectively. This maximum point occurs at approximately the 23 inch rod bank position. The accuracy of these measurements of heating rate in pure aluminum are  $\pm 6.2$ ,  $\pm 7.5$ , and  $\pm 8.1\%$  at the full-in position for the near, middle, and far cylinders, respectively, at the 95% confidence level. The full-in position is defined as the calorimeter position when the center of the aluminum cylinders are in the core North-South vertical midplane. Plots of nuclear heating rate as a function of distance along the HT-1 axis, distance along the axis perpendicular to the core vertical surface, and rod bank position are given in Figures 7-12. A plot of calorimeter accuracy as a function of heating rate is given in Figure 6. The accuracy of all measurements between 0 and 14.5 inches from full-in is  $\pm 10\%$  or better at the 95% confidence level.

### 3.0 DESCRIPTION OF CALORIMETER AND EXPERIMENT

#### 3.1 Calorimeter Description

The calorimeter used for these nuclear heating measurements consists of 3 aluminum cylinders (99.995% pure) as shown in Figure 2. One end of each cylinder is connected to a cover plate, the right side of which is maintained near cooling water temperature. The remaining surfaces of each cylinder are exposed to air at 1 mm of Hg pressure maintained inside the calorimeter container. The outer surface of the cover plate and calorimeter container are cooled with nominal 65 gpm, 130°F Plum Brook Reactor cooling water, which is directed past the assembly by a shroud. As a steady state gamma heating takes place in the cylinders, they develop a steady state temperature distribution with the hottest point at the end of the cylinder inside the container and the coldest point toward the wetted surface of the cover plate.

The nuclear heating rate is a function of cylinder  $\Delta T$  measured by 4 chromel-alumel thermocouples attached to each cylinder as shown in Figure 2 with the thermocouple identification number. The midpoint between the two sets of thermocouples is located at the core North-South vertical midplane, when the W2-3 capsule is inserted to the full-in position. The calorimeter assembly, which includes the cylinders, thermocouples, cover plate, and container, was designed and fabricated by the Idaho Nuclear Corporation (References 1-3).

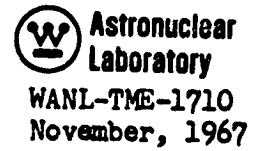
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### 3.1 (Cont'd)

More detail on the calorimeter assembly is found in Idaho Nuclear Corporation Drawings, Reference 4. More detail on the shroud and W2-3 capsule designed and fabricated by Westinghouse Astronuclear Laboratory is found in Reference 5.

### 3.2 Description of Test

The objective is to define the nuclear heating spatial distribution in HT-1 where experimental assemblies will be irradiated. This is shown in Figure 1. Specimens will usually be near the core North-South vertical midplane. The W2-3 capsule can be moved to any position between full-in and completely withdrawn. The spatial heating distribution was obtained along the HT-1 axis by taking measurements at the following distances from the full-in position: 0, 1, 3, 5, 8.5, 12, 13, 13.5, 14, 14.5, 15, 15.5, 16, 18, 20, 25, 30, 40, and 45 inches from the full-in position, the density of points increasing near 13.5 inches, the core boundary. The spatial heating distribution was obtained along a horizontal line perpendicular to the core vertical surface and intersecting the HT-1 axis by the use of three aluminum cylinders each separated by 2.5 inches in the horizontal plane containing the HT-1 axis. The above measurements were made on nine different days in the 65-P cycle, recording data described in Section 4.0 in each case.



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### 3.2 (Cont'd)

The contribution of background radiation to total nuclear heating was determined by inserting the calorimeter assembly to the full-in position after shutdown.

#### 4.0 DATA ACQUISITION

The data obtained in this experiment at each calorimeter position along the HT-1 axis are: date, time, reactor power (MW), time integrated power (MWD), core inlet and outlet temperatures, shim rod bank positions, regulator rod positions, temperatures of the 12 calorimeter thermocouples, the average temperature of each of the 12 calorimeter thermocouples during the period the calorimeter remained in a given position, the standard deviation of each calorimeter thermocouple temperature, the temperature of the calorimeter container, HT-1 water flow, the calorimeter container air pressure, and the calorimeter distance from full-in position. The PBRF Experiment Data Logger Acquisition System (EDLAS) recorded all the above data except the calorimeter container air pressure, one of the four calorimeter container thermocouples, and the calorimeter distance from full-in position. These three parameters were recorded in the Experiment Control Room (XCR), however.

The data logger (EDLAS) prints out data once every minute or on demand. Typical data logger printout is shown in APPENDIX A for each calorimeter position on September 13, 1967. The first column on the left is the date; the fourth column from the left (neglecting the column containing BA and that containing T) is the time; the fifth and sixth columns from the left contain the time integrated power and the power, respectively. These columns are numbered 29 and 30 as

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4.0 (Cont'd)

indicated by the number directly above the column. The columns to the right of these are numbered 32 through 85 as shown. Directly above the column number is a description of the parameter in that column and in some cases an indication of where the decimal point is to be placed. For example, 10-2 means multiply the value in that column by  $10^{-2}$  or put the decimal point two places to the left. If there is no such indication in the column heading, the decimal point is immediately to the right of the last digit on the right. There is one exception to this in column 61, HT-1 flow. Here the value should be multiplied by  $10^{-1}$ . Table 1 gives an explanation of each column with units. It should be noted that column 59, HT-1 inlet temperature, is really HT-1 outlet temperature and column 60, HT-1 outlet temperature is really HT-1 inlet temperature. A row is skipped between the data associated with each calorimeter position.

The following data were taken by Plum Brook WANL Test Operations personnel at each calorimeter position: reactor power, control rod bank position, calorimeter container air pressure, date, time, calorimeter distance from full-in position, HT-1 flow and temperatures, and one thermocouple on the calorimeter container. The calorimeter position (distance from full-in) was recorded beside the applicable data logger printout.

## 5.0 ANALYTICAL TECHNIQUES

The TOSS heat transfer code is used to describe the equilibrium temperature distribution in the cover plate and calorimeter cylinders, so that an accurate proportionality can be obtained between cylinder  $\Delta T$  and heating rate using a calculation that includes heat loss from cylinders by radiation and convection. A computer program was written to reduce the raw data and calculate nuclear heating from it. A set of criteria are discussed and used accepting only the reliable temperature data. The accuracy of this calorimeter is calculated and given as a function of nuclear heating rate. The nuclear heating rates normalised to 60 MW are fitted to equations describing the spatial distribution using a linear regression computer program.

### 5.1 TOSS Model

For the TOSS computer model (Reference 6) the calorimeter cylinder, cover plate, and fins are divided into 42 internal nodes (small volume elements), surface nodes associated with some of these internal nodes, and two boundary nodes 2001 and 2002 as shown in Figure 3. The computer calculates the steady state internal and surface temperatures of each node. The thermocouples are in nodes 4 and 10. Heat transfer is considered by conduction between nodes, from each of nodes 1-12 to the wall of the calorimeter container by convection and radiation, and from nodes 42, 50-62, 71, 73, 75, and 77 to the cooling water by forced convection.

5.2 (Cont'd)

Node 2001 is a boundary node that has the temperature of the inside wall of the calorimeter container (Figures 2 and 3). Node 2002 is a boundary node that has the bulk temperature of Plum Brook Reactor cooling water passing through T-1 and incident on the fins and cover plate. All nodes are given cylindrical symmetry with the axis of the center calorimeter. Thus, nodes 1-12, 21, and 50 are cylinders, while nodes 32-42, 51-62, 71, 73, 75, and 77 are cylindrical shells. Nodes 74, 73, 76, and 77 represent the fins, which are not in reality cylindrical shells but flat plates. Node 21 is a 2 mm thick air space to represent an interface between the end of the calorimeter cylinder and the bottom of the hole in the cover plate where the cylinder is inserted. The dimensions of each node are given in Table II. Cases are run for 7, 6, 5, 3, 1, and 0.2 watt/g-gram to obtain a relationship between heat generation rate and  $\Delta T$  across the calorimeter, which is the difference between node 4 and node 10 temperatures.

The input to TEC for each case consists of specifying a heat generation rate for each internal node, fixed boundary temperatures for boundary nodes 2001 and 2002, heat capacity and thermal conductivity of the aluminum and air (node 21), node dimensions with realistic lengths and areas for heat transfer, heat transfer coefficients for radiation or forced or free convection, and an estimate of the initial internal and surface node temperatures. The heat generation rate, which is

5.1 (Cont'd)

the same for all internal nodes except node 21 (which has essentially no heat generation rate), takes on values of 7, 6, 5, 3, 1, or 0.2 watts/gram depending on which case is being run. Node 21 is given zero heat generation rate; because the input to TOSS is in BTU/hr-in<sup>3</sup>, and the air density is so much smaller than the aluminum density that the volumetric heat generation rate in air is negligible. In reality, the heat generation rate is not uniform throughout the material in this TOSS model, and each node should have an individual heating rate. This uncertainty is accounted for in the accuracy analysis (Reference 1) for the cylinder itself. The above six cases are run for each of four different node 2002 temperatures: 120, 125, 130, and 135°F in order to provide a relationship between heat generation rate and  $\Delta T$  for all HT-1 inlet temperatures experienced during calorimeter heating rate measurements. Node 2001 temperature, which is also fixed throughout any given case, is the temperature of bulk cooling water (2002) plus the film rise plus the  $\Delta T$  across the 0.2815 inch thick calorimeter container wall.  $T_{2001} = T_{2002} + 4.31H$ .

Where  $H$  is the heat generation rate (watts/gram),

4.31 is the proportionality between  $\Delta T$  (film) +  $\Delta T$  (wall)  
and heat generation rate,

### 5.1 (Cont'd)

$$\Delta T (\text{film}) = q/h,$$

$q = (6.13 \times 10^3)H = \text{BTU/hr-ft}^2$  of heat flux coming out of the calorimeter container,

$$h = 1750 \text{ BTU/hr-ft}^2\text{-}^\circ\text{F},$$

$$\Delta T (\text{wall}) = QA/2k,$$

$$Q = (2.61 \times 10^5)H = \text{BTU/hr-ft}^3,$$

$$A = 5.50 \times 10^{-4} \text{ ft}^2,$$

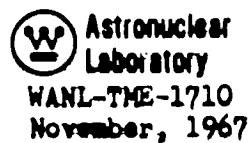
and  $k$  = thermal conductivity = 89.5 BTU/hr-ft- $^\circ\text{F}$ .

The thermal conductivity of pure aluminum is given in Table III and is taken from Reference 7. The thermal conductivity of air is assumed to be constant at 0.0157 BTU/hr-ft- $^\circ\text{F}$ . Heat transfer by radiation from nodes 1-12 to the calorimeter container wall is accomplished with the Stefan-Boltzmann radiation law using an emissivity of 0.3 (Reference 8, Table A-23, p. 472). This yields a radiation heat transfer coefficient that can be put into TOSS. The free convection heat transfer coefficient,  $h$ , to describe heat loss from nodes 1-12 by free convection is taken from McAdams (Reference 8), equation (7-6a):

$$h = \frac{0.53k_f}{D_o} \left[ \frac{\sum f^2 R_f}{\sum f} \right]^{1/2} \left( \frac{c_p f}{k} \right)^{1/2.5}$$

where  $k$  is the thermal conductivity of the air (BTU/hr-ft- $^\circ\text{F}$ ),

$D_o$  is the outside diameter of the calorimeter cylinder (ft),



### 5.1 (Cont'd)

$\rho$  is the air density ( $\text{lbs}/\text{ft}^3$ ),  
 $g$  is the acceleration of gravity ( $4.17 \times 10^8 \text{ ft}/\text{hr}^2$ ),  
 $\beta$  is the coefficient of volumetric expansion ( $^{\circ}\text{F}^{-1}$ ),  
 $\Delta t$  is the temperature difference ( $^{\circ}\text{F}$ ) between the cylinder surface and the bulk air,  
 $\mu$  is the viscosity of the air ( $\text{lbs}/\text{hr-ft}$ ),  
 $c_p$  is the specific heat of the air ( $\text{BTU}/\text{lbs-}^{\circ}\text{F}$ ),  
and the subscript,  $f$ , implies film property.

The air pressure in the calorimeter container was maintained at 1 mm of Hg  $\pm 5\%$ . A forced convection heat transfer coefficient,  $h_m$ , of 1750  $\text{BTU}/\text{hr-ft}^2-{}^{\circ}\text{F}$  was used for the cylindrical surfaces associated with nodes 42 and 62 (annular region). This coefficient was obtained from an equation used by McBride (Reference 9):

$$\left(\frac{h_m D_0}{k}\right)_b = 0.023 \left(N_{Re}\right)_b^{0.8} \left(N_{Pr}\right)_b^{0.4} \left(\frac{d_2}{d_1}\right)^{0.45}$$

where  $D_0 = d_2 - d_1 = (7.000 - 6.625) 1/12 = .03125 \text{ ft.}$ ,

$k = 0.374 \text{ BTU/hr-ft-}^{\circ}\text{F}$ ,

$$N_{Re} = \nu D_0 \rho / \mu = 30,530. = (5.14 \text{ ft/sec})(.03125 \text{ ft})(61.6 \text{ lbs}/\text{ft}^3)/ \\ (3.24 \times 10^{-4} \text{ lbs}/\text{ft-sec})$$

based on a flow of 63.7 gpm,

and  $N_{Pr} = 3.27$ .

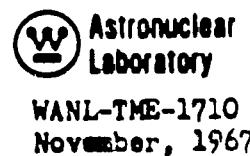
### 5.1 (Cont'd)

A film heat transfer coefficient in the vicinity of the fins was taken to be 500 BTU/hr-ft<sup>2</sup>-°F based on this same equation, using a  $\text{f}_{\text{c}}$  of 0.0104, ft<sup>2</sup> and a velocity of approximately 1 ft/sec. Then the film heat transfer coefficients for the surfaces associated with nodes 58-61 are simply chosen to be 600, 700, 800, 900, and 1000 BTU/hr-ft<sup>2</sup>-°F, respectively, as the velocity is increasing with the radius of the cover plate.

The output of TUE gives the steady state temperature distribution for the internal and surface nodes. There are a total of 24 output cases: 7, 6, 5, 3, 1, and 0.2 watts/gram at each of four 1/4-l cooling water bulk temperatures of 120, 125, 130, and 135°F. These temperature distributions yield a relationship between nuclear heating rate (watts/gram) and calorimeter  $\Delta T$  (°F) as a function of nuclear heating rate for a family of four different bulk cooling water temperatures. This is given in Table IV.

### 5.2 Computer Program to Reduce Data

The problem of calculating nuclear heating rate (watts/gram) from the raw data for each calorimeter position on each day that measurements were taken involves numerous calculations by hand. A computer program to reduce this data is given in "APPENDIX IV"; the reduced data is given in APPENDIX C.



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## 5.2 (Cont'd)

Each thermocouple was individually calibrated by the Idaho Nuclear Corporation. These calibration curves (in degrees C) are given in the Design Data Package, Reference 9. But the Plum Brook data logger prints out these temperatures (in degrees F) using the standard calibration from EMF to temperature for chromel-alumel thermocouples. So each temperature was corrected by converting the data logger temperature back to EMF (millivolts) using the standard calibration and then converting this EMF to temperature using the individual calibration by Idaho Nuclear. By hand, this in itself would involve reading two plots (the standard calibration curve and the applicable individual calibration curve) approximately 1400 times. One subroutine, FUNCTION EMF(T), converts data logger temperatures to EMF; another subroutine, CORRECT, converts this EMF back to temperature ( $^{\circ}$ F) using the individual calibration for the applicable thermocouples. This is accomplished in statements 12 through 80 in APPENDIX B.

Now the  $\Delta T$  associated with each calorimeter cylinder is obtained using accepted temperatures for each cylinder as discussed in Section 5.3. This is accomplished in statements 205, 215, and 225 in APPENDIX B for the near, middle, and far cylinders, respectively. Subroutine HDELT then converts the  $\Delta T$  to heating rate (watts/gram) using the appropriate

## 5.2 (Cont'd)

proportionality in Table IV. The heating rate of each cylinder is then normalized to 60 MW in statements 240, 250, and 260. APPENDIX C, the output of this program, is the reduced data for all calorimeter measurements made at power.

## 5.3 Temperature and Heating Data Acceptance

Examination of the reduced temperatures in APPENDIX C shows anomalous temperature data with some of the 12 calorimeter thermocouples. A pair of thermocouples is defined as two thermocouples at the same end of the same calorimeter cylinder (See Figure 2). APPENDIX C shows large temperature differences (such as 42, 24, and 46°F at full-in on September 13) between pairs 1 & 3, 6 & 8, and 10 & 12 respectively, for calorimeter positions near full-in. Only part of this temperature data can be accepted; therefore, a list of criteria are discussed for temperature acceptance.

### 5.3.1 Criteria For Temperature Acceptance

#### Criterion 1

When the calorimeter is sufficiently near the core (i.e. between 0 and 15 inches from full-in),  $H_n + H_m = H_f$ . Where  $H$  is heating rate (watts/gram), and the subscripts n, m, and f refer to near, middle, and far calorimeter cylinders, respectively. This may not be true at distances greater than 15 inches, because of such things as increasing complexity in attenuation geometries and an increasing ratio of secondary to prompt core gammas.

5.3.1 (Cont'd)

Criterion 2

$(T_n)_h > (T_m)_h > (T_f)_h$  and  $(T_n)_c > (T_m)_c > (T_f)_c$ .

Where T is temperature, the subscripts n, m, and f are the same as in Criterion 1, and the subscripts h and c refer to hot and cold end of a cylinder.

Criterion 3

When the calorimeter is between 0 and 15 inches from full-in,  $|S_{nm}| \geq |S_{mf}|$ . Where  $S_{nm}$  is the slope of  $\ln H$  between the near and middle cylinders and  $S_{mf}$  is the same slope between the middle and far cylinders. This criterion is supported by Plum Brook MUR (Mock-Up Reactor) measurements, Reference 10, Figures 4-6. It also has theoretical support, because functions used to describe fields from a plane source such as  $1/r$  or  $E_1(b)$  or  $E_2(b)$  in Rockwell's shielding manual (Reference 11) all satisfy this criterion.

Criterion 4

Electrical Integrity - Each thermocouple should be intact electrically, i.e., there should be no abnormal resistance or lack of continuity.

Criterion 5

TOSS Model - Measured temperatures should agree generally with those calculated using the TOSS model. Precise agreement may not

### 5.3.1 (Cont'd)

be possible for several reasons. First, the film heat transfer coefficients chosen for the surfaces of nodes 50, 52, 54, 56, 58-61, 71, 73, 75, and 77 are somewhat uncertain. Secondly, an accurate knowledge of calorimeter heat generation rate is dependent upon acceptance of only the reliable thermocouples. Finally, the TOSS model represents the middle calorimeter cylinder more closely than the near and far cylinders, which will experience some end effects or assymmetries for the temperature distribution in the region of the cover plate into which they are inserted.

### 5.3.2 Accepted Temperature Data

In the first attempt to accept only the reliable temperature data it was thought that in any pair of temperatures with large difference, the thermocouple with the high reading was in error, because its junction was not in good thermal contact with the aluminum cylinder. It would therefore be hotter for two reasons: (1) there is a longer path for conduction to the heat sink than exists for the aluminum cylinder and (2) the thermal conductivity of the stainless steel is lower than that for aluminum. Under this hypothesis, the accepted thermocouples are:

Cylinder	Thermocouple	
	Hot End	Cold End
Near	9	10
Middle	5 & 7	6
Far	1	2 & 4

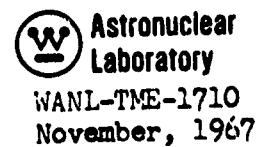
### 5.3.2 (Cont'd)

And the corresponding temperatures on September 11 at the full-in position are (from APPENDIX C):

<u>Cylinder</u>	<u>Corrected Temperature (°F)</u>	
	<u>Hot End</u>	<u>Cold End</u>
Near	465	277
Middle	401	260
Far	280	204

Using Table IV, this yields heating rates of 4.9, 3.65, and 1.95 watts/gm for the near, middle, and far cylinder respectively. Plotting this on semi-log paper shows that this set of temperature data does not satisfy Criterion 3.

Examination of the 12 temperatures plotted as a function of calorimeter distance from full-in position on a given day proves to be valuable in temperature data acceptance. Figures 4 and 5 are plots of the above temperatures on September 13; the thermocouple number itself is plotted. Temperatures have the same behavior on other days. It is seen from these figures that temperatures from thermocouples 2 and 4 are nearly equal at all calorimeter positions; the same is true with pair 5 & 7 as would be expected for all pairs. Pairs 6 & 8, and 9 & 11 show considerable spread. Pairs 1 & 3, and 10 & 12 also show considerable spread (approximately 50°F in each pair when calorimeter is near full-in position); but, in this case temperatures from thermocouples 1 and 10



### 5.3.2 (Cont'd)

are nearly equal at all calorimeter positions and so are temperatures from thermocouples 3 and 12. It is concluded from this that thermocouples 1 and 10 constitute a pair, and thermocouples 3 and 12 constitute a pair. Here, recall that a pair is defined as two thermocouples at the same end of the same cylinder. At this point there is still doubt as to which pair is to be associated with the hot end of the far cylinder and which pair to the cold end of the near cylinder. But after satisfying Criterion 4 as discussed in the next paragraph, it is seen that only if pair 1 and 10 is at the cold end of the near cylinder and pair 3 and 12 is at the hot end of the far cylinder can Criterion 3 be satisfied.

Electrical measurements, made by the PBRF WANL Test Operations group, of all 12 thermocouples are reported in Reference 12. Abnormalities are found in Table 3 of this reference, where a comparison is made between (1) the resistance across the entire thermocouple, i.e., resistance from chromel lead to alumel lead measured at the console in the containment vessel and (2) the sum of chromel to ground resistance and alumel to ground resistance measured at the same place. The latter value is always greater than the former value, but for thermocouples 3 and 11 this difference is 15.8 and 31.2 ohms, respectively. Table V of this document is taken from Table 3, Reference 11. It is seen that

### 5.3.2 (Cont'd)

thermocouples 3 and 11 have much greater differences than the others. Under a hypothesis that these differences for thermocouples 3 and 11 do not belong to the population of differences for the other 10 thermocouples, it is seen that at the 2 sigma level of significance  $-1.59 \leq$  difference  $\leq 8.25$  ohms for the 10 thermocouples, and the hypothesis should be accepted with better than 95% confidence.

After accepting thermocouples 1 and 10 as the pair at the cold end of the near cylinder, accepting thermocouples 3 and 12 as the pair at the hot end of the far cylinder, and not accepting the data from thermocouples 3 and 11 to satisfy Criterion 4, it is seen that all remaining thermocouples except number 8 can be accepted. The temperature from thermocouple 8 is higher than those from thermocouples 1 and 10, hence data from thermocouple 8 is not accepted so that Criterion 2 will be satisfied. The resulting temperature data used to calculate heat generation rate is as follows:

<u>Calorimeter Cylinder</u>	<u>Accepted Thermocouples</u>	
	<u>Hot End</u>	<u>Cold End</u>
Near	9	1 & 10
Middle	5 & 7	6
Far	12	2 & 4

Temperature data from the above thermocouples are used to calculate nuclear heating rates as shown in APPENDIX B and APPENDIX C.



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### 5.3.3 Accepted Heating Rate Data

Examination of APPENDIX C shows that the near and far cylinders give negative heating rates, when the calorimeter is 40 inches from the full-in position. It is concluded that heating rates at 40 inches from full-in are below the sensitivity of this calorimeter, and this position is not used in the regression analysis to determine the nuclear heating rate distribution along the HT-1 axis.

### 5.4 Accuracy Analysis

An accuracy analysis for this calorimeter is given in Reference 11, which considers all uncertainties affecting the calorimeter accuracy. But two such uncertainties were found to be larger than assumed in Reference 13. Both uncertainties pertain to the temperature data. First, the individual calibrations for each thermocouple are accurate to  $\pm 1.8^{\circ}\text{F}$  from Reference 9, whereas, they were assumed to be accurate to  $\pm 1.5^{\circ}\text{F}$  in the original accuracy analysis. Second, the temperature accuracy of a thermocouple system as measured by the data logger was taken to be  $\pm 1^{\circ}\text{F}$  in the accuracy analysis, but repeated readings at a given calorimeter position (APPENDIX A) show these temperatures to be accurate to  $\pm 1.6^{\circ}\text{F}$  at the 2 sigma confidence level. This is from an examination of all data logger prints out at calorimeter positions between zero and 13 inches from full-in, which shows that the standard deviation, sigma, for temperatures from accepted thermometers is  $\pm 0.16^{\circ}\text{F}$ .



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#### 5.4 (Cont'd)

to or less than  $3^{\circ}\text{F}$  approximately 95% of the time. Table VI gives all the heat generation rate uncertainties using the  $\pm 1.8$  and  $\pm 6^{\circ}\text{F}$  uncertainties in thermocouple calibration and data logger reading respectively; the table also gives combined calorimeter accuracy. This is the same as Table II, Reference 1), except for use of the above uncertainties in temperature. These accuracies range from  $\pm 6.1\%$  at 7 watts/gram to  $\pm 11\%$  at 0.2 watts/gram. The accuracy at the 95% confidence limit is plotted in Figure 6.

#### 5.5 Regression Analysis

The normalized nuclear heating rates are fitted to equations using a stepwise linear regression computer program. The equations have the form:

$$H(z) = a_0 + a_1 z + a_2 z^2 + a_3 z^3 \quad \text{for } 0 < z < 18 \text{ inches}$$

$$\ln H(z) = b_0 + b_1 z + b_2 z^2 + b_3 z^3 \quad \text{for } 18 < z < 30 \text{ inches}$$

$$\ln H(y) = c_0 + c_1 y + c_2 y^2 + c_3 y^3 \quad \text{for } -2.5 < y < 2.5 \text{ inches}$$

$$H(z) = d_0 + d_1 z + d_2 z^2 + d_3 z^3$$

where  $H$  is the nuclear heating rate (watts/gram),

$z$  is the distance from the full-in position (inches),  $z$  is the IT-1 axis in the case of the middle calorimeter cylinder,

$y$  is the horizontal line perpendicular to the core vertical surface intersecting the IT-1 axis at zero inches from full-in.

$y = -2.5$  in for the near cylinder, 0 inches for the middle cylinder, and 2.5 inches for the far cylinder.



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5.3 (Cont'd)

x is the control rod bank position (inches),  
and 18 inches is where  $H(x)$  changes from approximately a parabola to  
approximately an exponential.

If some of the above powers of the independent variable are  
insignificant the computer code will give no dependency on them.

## 6.0 RESULTS

Results are given for the spatial heating distribution, the heating distribution as a function of reactor control rod bank position, and the heating after reactor shutdown. The accuracy of these measurements are given as a function of nuclear heating rate.

### 6.1 Heating Distribution Along MT-1 Axis, $H(s)$

The regression analysis gives, for  $H(s)$  between 0 and 18 inches from full-in, the following equations for the near, middle, and far cylinders, respectively.

$$H_n(s) = 4.937 + (6.775 \times 10^{-2})s - (1.749 \times 10^{-2})s^2 + (1.603 \times 10^{-4})s^3.$$

$$H_m(s) = 3.725 + (6.606 \times 10^{-2})s - (1.440 \times 10^{-2})s^2 + (1.929 \times 10^{-4})s^3.$$

$$H_f(s) = 3.118 + (5.124 \times 10^{-2})s - (1.141 \times 10^{-2})s^2 + (1.528 \times 10^{-4})s^3.$$

For  $18 \leq s \leq 30$  inches the regression analysis gives:

$$\ln H_n(s) = 4.405 - 0.2216s.$$

$$\ln H_m(s) = 3.203 - 0.1793s + (1.118 \times 10^{-3})s^2,$$

$$\ln H_f(s) = 0.00297 + (7.403 \times 10^{-3})s^2 - (3.716 \times 10^{-4})s^3.$$

or

$$H_n(s) = 81.86 \exp(-.2216s).$$

$$H_m(s) = 24.65 \exp\left[-.1793s + (1.118 \times 10^{-3})s^2\right].$$

$$H_f(s) = 1.00297 \exp\left[(7.403 \times 10^{-3})s^2 - (3.716 \times 10^{-4})s^3\right].$$

These functions are plotted in Figures 7-10, where the dashed lines indicate the limits of accuracy of the measurement at the 95% confidence level. These equations represent all data taken during the cycle.

### 6.1 (Cont'd)

It is seen from Figure 10 that, when  $s = 20$  inches, the middle calorimeter cylinder gives a higher heating rate than the near cylinder. This may be due to such things as the increasing complexity of attenuation geometries and an increasing ratio of secondary gammas to prompt core gammas, but since the uncertainty beyond  $s = 20$  inches is  $\pm 25\%$  or greater, there is not much statistical significance in this fact. The sensitivity of this calorimeter at low heating rates had to be compromised in the design in order to provide capability of measuring a maximum of 7 watts/gm, the upper limit in the envelope of predicted nuclear heating for the near cylinder as shown in Figure 5, Reference 14.

### 6.2 Heating Distribution Along Horizontal Line Perpendicular to Core Vertical Surface, $H(y)$

The regression analysis gives the following expression for  $H(y)$ :

$$\ln H(y) = 1.351 - 0.09229y,$$

or  $H(y) = 3.87 \exp(-.09229y).$

This is plotted in Figure 11, and it has a value of 3.87 watts/gm at  $y = 0$  (on the  $z=1$  axis) and a value of 4.00 watts/gm at  $y = -2.5$  inches. These values represent the average of all measurements at the null-in position, hence they can be considered an average for the cycle.

### 6.3 Heating Vs. Rod Bank Position

The regression analysis gives the following expressions for nuclear heating as a function of rod bank position for the near, middle, and far cylinders, respectively, at  $z = 0$ :

$$H_n(x) = 3.554 + 0.09410x - (5.876 \times 10^{-5})x^3,$$

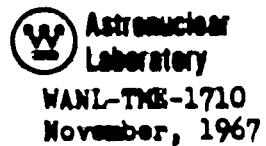
$$H_m(x) = 2.783 + 0.06414x - (3.958 \times 10^{-5})x^3,$$

$$H_f(x) = 2.273 + 0.03670x - (3.494 \times 10^{-5})x^3.$$

These are plotted in Figure 12, and it is seen that the maximum heating rate occurs at approximately the 23 inch rod bank position. Here heating rates are 3.00, 3.78, and 3.15 watts/gm for the near, middle, and far cylinders, respectively at the full-in position.

### 6.4 Heating After Shutdown

The heating rate on September 13 between 11:31 p.m. and 11:49 p.m., 2 hours after reactor shutdown, was .066 watts/gm for the near cylinder, 0.26 watts/gm for the middle cylinder, and negative for the far cylinder. This is in the region where the calorimeter cylinders are accurate to the order of  $\pm 100\%$ . Hence, it is concluded that any heating after shutdown from fission product decay or active isotopes in the surrounding media is below the sensitivity of the calorimeters.



## 7.0 CONCLUSIONS & RECOMMENDATIONS

The following conclusions and recommendations are made.

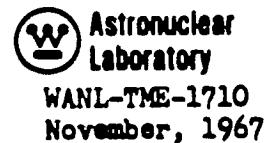
1. This calorimeter is usable between 7 and 1.7 watts/gm at an accuracy of  $\pm 15\%$  or better at the 95% confidence level. For accuracies of  $\pm 10\%$  or better it is usable between 7 and 2.7 watts/gm.
2. The objectives of this experiment were accomplished successfully, as nuclear heating in pure aluminum was measured to within  $\pm 10\%$  or better (95% confidence level) at positions between 0 and 14.5 inches from full-in.
3. It is recommended that the values of nuclear heating in pure aluminum given in this document be used for HT-1 with the accuracy indicated in Figure 6, until further measurements are made.
4. Further measurements could improve the accuracy at 3 watts/gm to  $\pm 5\%$  (95% confidence level) at best by designing a new calorimeter that would reduce the temperature uncertainties to  $\pm 1$  to  $1.5^{\circ}\text{F}$ .
5. If a new calorimeter is designed copper-constantan thermocouples are recommended for use instead of chromel-alumel, because there should be less uncertainty by virtue of greater EMF.
6. Also, if a new calorimeter is used, it is recommended that the one used in this experiment be disassembled and examined for causes

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7.0 (Cont'd)

of the anomalous temperature data. Otherwise, it is recommended that this calorimeter remain intact for future use.

7. The sensitivity of a new calorimeter can be extended to lower heating rates, because the upper limit in the envelope of predicted nuclear heating is now only 5 watts/gm plus 6.5% or 5.33 watts/gm at the 95% confidence level.



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APPENDIX A

Typical Data Logger Printout

Attached is the data logger printout of September 13, which is typical of data logger printout on the other days. Also included is the printout for the three sets of data on September 13 and 14 after reactor shutdown. APPENDIX C lists all data from data logger printout for each day at power except the standard deviation, sigma, associated with each set of temperature data.

LOG HEADING	ACC PWRT	MWD MW	SR 1	SR 2	SR 3	SR 4	SR 5	SR 6	SR 7	SR 8	RR 1	RR 2	TC01	TC02	TC03	TC04	TC05	TC06	TC07	TC08	
			INLT	OUTL	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	PER	PER	FAR	FAR	FAR	FAR	MID	MID	MID	MID	
			F	F	10-2	10-2	10-2	10-2	10-2	10-2	CENT	CENT	HOT	COLD	HOT	COLD	HOT	COLD	HOT	COLD	
10-1	10-1																				
SE13 BA H 0900 0029 0030			0032	0033	0034	0035	0036	0037	0038	0039	0040	0041	0042	0043	0044	0045	0046	0047	0048	0049	0050
SE13 BA T 0910 7202 0602	0130	0157	2969	2969	2970	2967	2969	2970	2969	2970	0081	0088	0139	0142	0140	0141	0140	0138	0137	01	
SE13 BA T 0911 7202 0601	0130	0157	2969	2968	2970	2967	2969	2970	2970	2970	0081	0088	0140	0141	0137	0137	0135	0135	0139	01	
SE13 BA T 0912 7202 0602	0130	0157	2969	2968	2970	2967	2969	2969	2970	2969	0081	0088	0143	0145	0139	0135	0136	0135	0140	01	
SE13 BA T 0913 7202 0602	0130	0157	2969	2968	2970	2967	2969	2970	2970	2970	0081	0088	0140	0141	0137	0137	0141	0140	0140	01	
SE13 BA T 0914 7202 0601	0130	0157	2969	2968	2970	2967	2969	2970	2971	2970	0081	0088	0141	0142	0135	0135	0135	0137	0137	01	
SE13 BA T 0915 7202 0601	0130	0157	2969	2968	2970	2967	2969	2970	2970	2969	0081	0088	0137	0142	0139	0140	0141	0140	0138	01	
SE13 BA T 0916 7202 0599	0130	0157	2969	2968	2970	2967	2959	2970	2970	2970	0081	0088	0138	0142	0140	0140	0140	0136	0136	01	
SE13 BA T 0917 7202 0600	0130	0157	2969	2968	2969	2967	2969	2970	2970	2969	0081	0088	0142	0142	0136	0136	0140	0141	0140	01	
SE13 BA T 0918 7202 0598	0130	0157	2969	2968	2969	2967	2969	2970	2970	2970	0081	0088	0137	0142	0139	0140	0141	0139	0138	01	
SE13 BA T 0919 7202 0597	0130	0157	2975	2969	2970	2967	2969	2969	2970	2970	0081	0088	0138	0143	0141	0141	0140	0137	0136	01	
SE13 BA T 0927 7206 0599	0130	0157	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0139	0144	0143	0141	0141	0137	0137	01	
SE13 BA T 0928 7206 0600	0130	0157	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0139	0143	0143	0140	0141	0137	0143	01	
SE13 BA T 0929 7206 0599	0130	0157	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0144	0147	0141	0137	0138	0136	0141	01	
SE13 BA T 0930 7210 0599	0130	0157	2980	2979	2980	2978	2979	2979	2980	2980	0079	0088	0142	0145	0142	0141	0141	0135	0139	01	
SE13 BA T 0931 7210 0602	0130	0157	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0142	0143	0138	0136	0141	0142	0142	01	
SE13 BA T 0932 7210 0601	0130	0157	2978	2978	2979	2978	2979	2979	2981	2980	0079	0088	0143	0144	0138	0136	0139	0140	0143	01	
SE13 BA T 0933 7210 0600	0130	0157	2977	2978	2980	2978	2979	2979	2980	2980	0079	0088	0143	0147	0139	0140	0139	0140	0142	01	
SE13 BA T 0934 7210 0601	0130	0157	2978	2978	2979	2978	2979	2979	2981	2980	0079	0088	0138	0142	0140	0140	0142	0140	0139	01	
SE13 BA T 0935 7210 0600	0130	0158	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0140	0141	0138	0139	0142	0140	0141	01	
SE13 BA T 0936 7210 0600	0130	0157	2978	2978	2980	2978	2979	2979	2981	2980	0079	0088	0139	0144	0143	0141	0141	0137	0138	01	
SE13 BA T 0943 7214 0603	0131	0158	2978	2978	2980	2978	2979	2979	2980	2980	0080	0088	0145	0150	0152	0142	0149	0141	0148	01	
SE13 BA T 0944 7214 0603	0131	0158	2978	2978	2979	2978	2979	2979	2981	2980	0080	0088	0148	0150	0150	0139	0149	0143	015	01	
SE13 BA T 0945 7214 0601	0131	0158	2978	2978	2980	2978	2979	2979	2981	2980	0080	0088	0148	0150	0150	0140	0149	0152	0150	01	
SE13 BA T 0946 7214 0600	0131	0158	2978	2978	2980	2978	2979	2979	2981	2980	0080	0088	0148	0150	0150	0140	0149	0152	0151	01	
SE13 BA T 0947 7214 0601	0131	0158	2978	2978	2980	2978	2979	2979	2981	2980	0080	0088	0148	0150	0150	0140	0149	0152	0152	01	
SE13 BA T 0948 7214 0601	0131	0158	2978	2979	2980	2978	2979	2979	2981	2980	0080	0088	0143	0150	0153	0143	0150	0141	0149	01	
SE13 BA T 0949 7214 0603	0131	0158	2978	2979	2980	2978	2979	2979	2981	2980	0080	0088	0142	0149	0153	0143	0150	0142	0148	01	
SE13 BA T 0950 7219 0601	0131	0158	2978	2979	2979	2978	2979	2979	2981	2980	0080	0088	0143	0144	0148	0142	0154	0152	0152	01	
SE13 BA T 0951 7219 0600	0131	0158	2978	2978	2980	2978	2979	2979	2980	2980	0080	0088	0147	0150	0152	0141	0148	0142	0150	01	
SE13 BA T 0952 7219 0602	0131	0158	2978	2978	2980	2978	2979	2979	2980	2980	0080	0088	0145	0147	0149	0142	0154	0146	0150	01	
SE13 BA T 1029 7231 0602	0132	0159	2988	2987	2989	2987	2989	2990	2990	2989	0080	0088	0150	0157	0165	0149	0173	0156	0170	01	
SE13 BA T 1030 7235 0599	0132	0158	2988	2988	2989	2987	2990	2990	2990	2990	0080	0088	0156	0158	0160	0147	0167	0150	0168	01	
SE13 BA T 1031 7235 0602	0132	0158	2988	2987	2990	2987	2989	2990	2990	2989	0080	0088	0154	0154	0165	0146	0169	0155	0173	01	
SE13 BA T 1032 7235 0599	0132	0159	2988	2988	2989	2987	2989	2990	2990	2989	0080	0088	0150	0157	0170	0150	0169	0150	0168	01	
SE13 BA T 1033 7235 0598	0132	0159	2988	2987	2989	2987	2989	2990	2990	2989	0081	0088	0156	0157	0167	0147	0167	0150	0170	01	
SE13 BA T 1034 7235 0598	0132	0159	2988	2987	2989	2987	2989	2990	2990	2989	0081	0088	0157	0157	0167	0146	0169	0150	0173	01	
SE13 BA T 1035 7235 0599	0132	0159	2988	2988	2989	2987	2989	2990	2990	2989	0081	0088	0153	0158	0160	0149	0169	0168	0168	01	
SE13 BA T 1036 7235 0601	0132	0159	2988	2988	2989	2987	2989	2990	2990	2989	0081	0088	0156	0154	0165	0146	0169	0155	0173	01	
SE13 BA T 1037 7235 0600	0132	0159	2997	2999	2999	2997	2999	2999	2990	2990	0079	0088	0150	0156	0169	0150	0173	0152	0167	01	
SE13 BA T 1038 7235 0600	0132	0159	2997	2999	2999	2997	2999	2999	3000	2999	0079	0088	0150	0157	0169	0150	0170	0150	0168	01	

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10. TIC TIC TICN TICG TICB TICD TICF TICJ TICL TICM TICN TICP TICQ TICR TICU TICV TICW TICX TICY TICZ TICAA TICBB TICCC TICDD TICEE TICFF TICGG TICHH TICJJ TICLL TICMM TICNN TICPP TICQQ TICRR TICUU TICVV TICWW TICXX TICYY TICZZ TICAAA TICBBB TICCCC TICDDD TICEEE TICFFF TICGGG TICHHH TICJJJ TICLLL TICMMM TICNNN TICPPP TICQQQ TICRRR TICUUU TICVVV TICWWW TICXXX TICYYY TICZZZ

三

0000	1110	0000	1110	0000	1170	0000	1370	0000	1360	0000	1470	0000	1400	0000	1420	0000	1420	0000
0001	1105	0000	1110	0000	1170	0000	1400	0100	1370	0150	1460	0100	1370	0200	1410	0100	1365	0250
0002	1107	0170	1100	0111	1167	0000	1403	0250	1370	0214	1470	0163	1463	0210	1407	0101	1387	0260
0003	1108	0163	1103	0129	1161	0002	1400	0223	1395	0216	1450	0192	1458	0216	1400	0102	1388	0260
0004	1108	0187	1104	0200	1160	0123	1172	0006	1400	0217	1390	0207	1460	0176	1470	0204	1400	0107
0005	1111	0156	1121	0221	1142	0126	1177	0016	1405	0213	1398	0196	1395	0160	1477	0217	1407	0101
0006	1111	0157	1121	0220	1142	0125	1176	0015	1400	0207	1400	0165	1460	0151	1477	0214	1405	0101
0007	1111	0158	1121	0219	1142	0124	1175	0014	1405	0203	1395	0217	1394	0164	1477	0221	1406	0101
0008	1111	0159	1121	0218	1142	0123	1174	0013	1408	0198	1382	0220	1391	0162	1476	0221	1407	0101
0009	1111	0160	1121	0217	1142	0122	1173	0012	1405	0201	1390	0213	1398	0155	1478	0221	1408	0101

1	111	1420	0000	1440	0000	1440	0000	1450	0000	1520	0000	1430	0000	1500	0000	1460	0000
2	110	1400	0000	1420	100	1405	0050	1460	0150	1505	0150	1420	0100	1440	0100	1470	0100
3	1106	1417	0211	1500	0141	1433	0211	1503	0208	1457	0170	1487	0207	1411	0150	1490	0061
4	0006	141	0132	1498	0129	1428	0204	1506	0192	1463	0178	1460	0210	1415	0111	1430	0070
5	0034	1411	0178	1496	0123	1424	0179	1510	0178	1464	0166	1460	0226	1416	0102	1430	0061
6	0126	1411	0101	1447	0111	1422	0108	1507	0102	1457	0221	1468	0205	1420	0129	1495	0125
7	0130	1416	0177	1497	0106	1421	0173	1503	0191	1451	0041	1490	0192	1421	0103	1499	0150
8	0116	1416	0165	1503	0171	1425	0167	1505	0187	1444	0236	1465	0282	1420	0150	1499	0136
9	0139	1416	0150	1500	0176	1426	0177	1504	0179	1451	0233	1467	0216	1421	0146	1498	0143
10	0161	1416	0159	1504	0201	1428	0200	1508	0192	1451	0222	1464	0211	1422	0143	1492	0142

0010	1120	0000	1110	0000	1560	0000	1700	0000	1540	0000	1620	0000	1470	0000	1700	0000	1680	0000
0150	1460	0100	1200	0200	1510	0300	1690	0100	1560	0200	1650	0100	1455	0150	1695	0050	1650	0300
0111	1471	0142	1697	0219	1517	0261	1703	0211	1567	0198	1650	0241	1477	0176	1691	0050	1671	0252
0212	1460	0158	1695	0217	1526	0277	1690	0204	1560	0200	1635	0229	1485	0238	1701	0161	1640	0216
0189	1478	0150	1690	0219	1522	0273	1698	0105	1566	0215	1656	0206	1490	0219	1700	0154	1642	0225
0112	1475	0150	1690	0206	1518	0262	1701	0200	1570	0216	1658	0198	1492	0206	1698	0148	1617	0235
0164	1477	0169	1699	0169	1514	0263	1700	0207	1569	0206	1620	0193	1496	0216	1703	0173	1639	0226
0169	1475	0150	1689	0176	1516	0271	1704	0217	1570	0193	1659	0176	1491	0231	1701	0169	1639	0208
0173	1474	0165	1693	0211	1519	0256	1700	0240	1567	0207	1659	0171	1498	0236	1704	0201	1642	0221
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7 T008 TC09 TC10 TC11 TC12 TC13 TC14 TC15 HT-1 HT-1 T001 TC01 TC02 T003 TC03 TC04 TC05 TC06 T007 TC07 TC08 TC09 TC09  
 MID NEAR NEAR NEAR NEAR FXT FXT FXT FXT OUTL FLOW AVG SIGM  
 COLD HOT COLD HOT COLD NEAR BOT FAR TEMP TEMP 10-1 10-2 10-1 10-2 10-1 10-2 10-1 10-2 10-1 10-2 10-1 10-2 10-1 10-2  
 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079  
 0183 0215 0169 0222 0197 0135 0136 0137 0142 0135 0061 1790 0000 1700 0000 2040 0000 1600 0000 2140 0000 1730 0000 2130 0000 1810 0000 2150 0000  
 0178 0211 0170 0227 0202 0135 0135 0137 0140 0135 0061 1710 0000 1600 0150 2050 0160 2020 2160 3200 1735 0050 2125 0050 1805 0250 2130 0200  
 0179 0210 0167 0225 0203 0135 0137 0139 0131 0062 1705 0267 1670 2040 2051 0208 1620 0163 2170 0216 1747 0170 2133 0130 2000 0216 2120 0216  
 0183 0212 0167 0221 0199 0136 0139 0131 0141 0131 0063 1715 0304 1670 0212 2033 0142 1613 0192 2168 0192 1753 0178 2165 0229 1808 0227 2120 0187  
 0177 0211 0169 0227 0202 0135 0136 0140 0135 0064 1708 0308 1660 0150 2050 0179 0179 1616 0208 2170 0178 1758 0164 2144 0206 1800 0254 2118 0178  
 0178 0211 0167 0227 0201 0136 0137 0140 0131 0061 1705 0300 1667 0179 2011 0163 1622 0201 2173 0179 1757 0160 2143 0180 1797 0263 2117 0160  
 0183 0210 0170 0225 0139 0136 0137 0143 0131 0062 1710 0320 1670 0277 2036 0162 1620 0198 2171 0173 1753 0176 2141 0184 1801 0253 2123 0211  
 0182 0212 0165 0221 0202 0137 0137 0140 0130 0061 1713 0307 1674 0261 2033 0171 1616 0205 2174 0172 1756 0166 2145 0144 1804 0244 2123 0198  
 0183 0216 0170 0225 0199 0136 0136 0143 0137 0064 1717 0313 1660 0303 2033 0165 1616 0195 2172 0171 1753 0198 2143 0168 1807 0246 2127 0222  
 0183 0216 0170 0225 0199 0136 0137 0143 0137 0061 1720 0313 1662 0276 2035 0162 1615 0195 2171 0165 1751 0199 2142 0165 1809 0244 2130 0238  
 0198 0246 0165 0240 0223 0136 0139 0138 0145 0132 0061 1810 0000 1710 0000 2210 0000 1600 0000 2150 0000 1910 0000 2140 0000 1980 0000 2160 0000  
 0198 0243 0179 0220 0136 0139 0137 0140 0131 0061 1800 0100 1700 0000 2210 0000 1600 0000 2150 0000 1915 0050 2155 0050 1970 0100 2145 0150  
 0198 0244 0179 0220 0218 0136 0139 0136 0140 0131 0061 1800 0160 1700 2207 0040 1600 0000 2147 0040 1913 0060 2140 0060 1971 0106 2143 0125  
 0199 0246 0162 0245 0218 0136 0139 0136 0140 0135 0062 1805 0165 1705 2201 0214 1605 0066 2145 0070 1913 0043 2143 0043 1978 0106 2144 0129  
 0241 0183 0262 0221 0136 0137 0136 0144 0135 0061 1820 0178 1760 126 2228 0215 1678 0273 2150 0103 1906 0137 2134 0111 1970 0178 2146 0123  
 0196 0247 0183 0261 0219 0138 0137 0142 0134 0061 1800 0160 1700 206 2215 0207 1602 0261 2148 0109 1997 0265 2132 0106 1968 0169 2150 0141  
 0200 0246 0182 0255 0218 0135 0139 0139 0140 0132 0062 1803 0159 1764 215 2214 0200 1677 0266 2147 0103 1993 0244 2134 0119 1973 0193 2051 0137  
 0195 0247 0163 0261 0220 0135 0136 0141 0137 0061 1848 0147 1768 216 2233 0275 1600 0259 2149 0103 1999 0252 2131 0136 1970 0193 2054 0140  
 0199 0246 0182 0255 0218 0135 0139 0139 0141 0132 0062 1802 0158 1769 209 2230 0263 1677 0263 2144 0103 1989 0248 2133 0143 1972 0193 2054 0138  
 0247 0183 0261 0219 0136 0137 0137 0142 0134 0061 1851 0160 1751 0209 2241 0268 1678 0253 2147 0103 1995 0253 2132 0140 1970 0194 2056 0138  
 0212 0277 0194 0233 0236 0136 0139 0139 0144 0131 0060 2000 0200 1710 0000 2420 0000 1740 0000 2130 0000 2040 0000 2690 0000 2120 0000 2770 0000  
 0214 0279 0175 0252 0136 0140 0139 0142 0133 0063 2010 0100 1810 0200 2015 0090 1720 0200 2715 0150 2020 0200 2695 0050 2130 0100 2760 0100  
 0213 0279 0195 0253 0136 0140 0139 0141 0131 0062 2020 0140 1867 0169 2027 0173 1760 0326 2723 0177 2023 0170 2700 0061 2130 0061 2760 0061  
 0212 0277 0194 0253 0236 0136 0139 0139 0140 0131 0060 2003 0108 1810 0200 2027 0150 1760 0262 2725 0150 2028 0163 2696 0062 2126 0062 2776 0062  
 0215 0279 0197 0256 0234 0135 0139 0140 0145 0134 0063 2006 0211 1816 0215 2026 0141 1760 0252 2718 0194 2020 0209 2696 0064 2126 0117 2132 0099  
 0213 0281 0199 0255 0235 0136 0138 0138 0143 0133 0064 2007 0213 1820 0216 2028 0138 1763 0261 2713 0205 2013 0244 2692 0125 2132 0107 2105 0138  
 0215 0279 0199 0255 0239 0136 0137 0137 0142 0132 0061 2010 0210 1823 0213 2430 0150 1763 0223 2710 0207 2010 0239 2693 0117 2134 0120 2105 0133  
 0212 0277 0194 0253 0241 0136 0139 0139 0140 0131 0061 2009 0216 1819 0226 2430 0122 1763 0210 2715 0234 2014 0244 2693 0106 2133 0119 2768 0131  
 0213 0278 0194 0256 0236 0137 0140 0139 0141 0131 0060 2010 0214 1818 0216 2426 0131 1762 0199 2714 0223 2016 0236 2694 0119 2132 0116 2763 0127  
 0215 0273 0200 0235 0237 0136 0138 0137 0142 0135 0063 2011 0214 1817 0206 2424 0170 1762 0190 2716 0217 2015 0224 2694 0112 2134 0124 2764 0123  
 0221 0107 0211 0323 0253 0136 0137 0139 0143 0135 0061 2100 0000 1870 0000 2600 0000 1830 0000 2950 0000 2100 0000 2870 0000 2210 0000 3070 0000  
 0227 0306 0203 0322 0251 0136 0141 0140 0141 0131 0062 2120 0200 1865 0050 2570 0300 1805 0250 2955 0050 2125 0250 2900 0300 2240 0300 3065 0050  
 0223 0304 0207 0325 0255 0137 0140 0140 0146 0136 0063 2117 0170 1871 0129 256, 0262 1800 0216 2553 0125 2133 0218 2907 0264 2237 0249 3071 0129  
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 0226 0305 0205 0322 0253 0136 0140 0140 0140 0131 0061 2116 0160 1874 0222 2563 0306 1802 0232 2552 0100 2132 0223 2904 0213 2236 0252 3058 0122  
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 0227 0312 0211 0324 0250 0135 0136 0139 0147 0136 0062 2115 0126 1864 0216 2577 0267 1807 0239 2561 0138 2126 0222 2697 0238 2239 0254 3073 0260  
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 0223 0311 0212 0325 0254 0135 0139 0138 0146 0135 0062 2117 0162 1862 0223 2580 0282 1809 0226 2550 0161 2126 0236 2694 0218 2240 0235 3062 0260  
 0220 0306 0210 0327 0254 0137 0139 0138 0141 0133 0063 2116 0162 1863 0216 2581 0270 1811 0222 2550 0154 2126 0243 2695 0206 2236 0254 3060 0260  
 0230 0331 0220 0350 0266 0137 0140 0141 0141 0134 0062 2190 0000 1890 0000 2700 0000 1870 0000 3130 0000 2210 0000 3050 0000 2700 0000 3310 0000  
 0236 0333 0218 0346 0261 0136 0141 0141 0141 0133 0061 2230 0100 1910 0200 2605 0150 1855 0250 3120 0100 2195 0150 3050 0300 2330 0100  
 0232 0332 0221 0349 0265 0136 0140 0140 0141 0139 0061 2220 0395 1917 0191 2693 0177 1850 0216 3123 0100 2193 0130 3070 0262 2327 0249 3320 0061  
 0236 0332 0217 0357 0262 0136 0142 0140 0140 0131 0061 2230 0373 1920 0173 2685 0176 1850 0254 3123 0062 2195 0129 3063 0326 2335 0259 3320 0070  
 0233 0329 0218 0349 0267 0137 0141 0140 0141 0135 0061 2224 0340 1914 0190 2680 0179 1854 0252 3128 0136 2208 0176 3064 0257 2334 0237 3318 0139  
 0236 0333 0220 0347 0261 0136 0140 0141 0141 0135 0062 2232 0354 1918 0203 2681 0160 1862 0228 3123 0161 2200 0162 3067 0275 2335 0238 3317 0137  
 0231 0331 0217 0346 0260 0136 0141 0141 0141 0136 0062 2230 0329 1920 0192 2683 0157 1860 0213 3123 0151 2203 0168 3063 0272 2337 0220 3316 0136  
 0233 0331 0221 0349 0261 0135 0140 0142 0136 0062 2228 0315 1923 0193 2684 0172 1863 0210 3123 0159 2200 0167 3060 0261 2336 0205 3319 0135  
 0236 0334 0218 0345 0264 0137 0142 0142 0133 0062 2231 0315 1923 0193 2685 0171 1860 0210 3121 0139 2209 0176 3063 0260 2339 0206 3321 0133  
 0236 0334 0219 0346 0261 0136 0141 0141 0141 0136 0061 2235 0320 1925 0160 2684 0163 1869 0203 3121 0131 2190 0178 3065 0266 2341 0209 3322 0138

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TC02	TC02	TC03	TC03	TC04	TC04	TC05	TC05	TC06	TC06	TC07	TC07	TC08	TC08	TC09	TC09	TC10	TC10	TC11	TC11	TC12	TC12
Avg	SIGM																				
10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2
0064	0065	0066	0067	0068	0069	0070	0071	0072	0073	0074	0075	0076	0077	0078	0079	0080	0081	0082	0083	0084	0085
1700	0000	2040	0000	1600	0000	2140	0000	1730	0000	2130	0000	1830	0000	2150	0000	1690	0000	2220	0000	1970	0000
1685	0150	2050	0100	1620	0200	2160	0200	1735	0050	2125	0050	1805	0250	2130	0200	1695	0050	2245	0250	1995	0250
1670	0244	2057	0208	1620	0163	2170	0216	1747	0176	2133	0130	1800	0216	2120	0216	1687	0134	2247	0208	2007	0261
1670	0212	2033	0132	1611	0192	2168	0192	1753	0178	2145	0229	1808	0227	2160	0187	1683	0129	2238	0238	2003	0218
1660	0194	2054	0179	1618	0204	2170	0178	1754	0164	2144	0206	1800	0252	2118	0172	1684	0127	2244	0250	2006	0229
1667	0179	2053	0163	1622	0203	2173	0179	1757	0160	2143	0183	1797	0213	2117	0160	1682	0121	2248	0248	2012	0241
1676	0277	2036	0162	1620	0192	2171	0173	1753	0176	2141	0184	1801	0253	2123	0211	1680	0130	2249	0230	2009	0237
1674	0264	2033	0171	1616	0205	2174	0172	1756	0186	2145	0143	1804	0244	2123	0198	1680	0165	2244	0249	2010	0233
1680	0105	2033	0165	1616	0195	2172	0171	1751	0194	2143	0188	1807	0246	2127	0222	1682	0170	2244	0237	2008	0221
1682	0246	2035	0162	1615	0175	2171	0165	1751	0199	2142	0185	1809	0244	2130	0232	1684	0171	2245	0226	2006	0215
1710	0000	2210	0000	1660	0000	2150	0000	1910	0000	2440	0000	1980	0000	2460	0000	1850	0000	2600	0000	2230	0000
1710	0000	2210	0000	1660	0000	2150	0000	1915	0050	2445	0050	1770	0100	2145	0150	1620	0300	2575	0250	2215	0150
1731	0100	2207	0048	1660	0000	2147	0048	1913	0068	2440	0061	1773	0106	2143	0129	1610	0262	2577	0268	2203	0206
1748	0249	2220	0234	1665	0086	2145	0070	1913	0043	2130	0082	1778	0108	2440	0129	1813	0248	2570	0212	2190	0208
1744	146	2228	0265	1678	0273	2150	0109	1906	0137	2434	0111	1770	0178	2446	0123	1818	0248	2560	0275	2200	0189
1748	0206	2206	0215	1682	0261	2148	0109	1907	0245	2132	0106	1968	0169	2150	0141	1821	0250	2585	0275	2198	0180
1744	0215	2215	0266	1677	0266	2147	0105	1893	0244	2434	0119	1973	0193	2151	0137	1823	0248	2580	0282	2196	0180
1748	0216	2216	0273	1660	0259	2149	0105	1864	0252	2411	0136	1970	0193	2154	0140	1826	0232	2580	0282	2196	0165
1749	0209	2230	0263	1677	0263	2148	0105	1869	0238	2433	0143	1972	0193	2154	0135	1826	0228	2580	0266	2194	0167
1751	0201	2241	0260	1678	0253	2147	0102	1865	0251	2132	0140	1970	0194	2156	0136	1828	0228	2581	0267	2194	0156
1740	0000	2420	0000	1740	0000	2730	0000	2040	0000	2690	0000	2120	0000	2770	0000	1940	0000	2930	0000	2380	0000
1710	0200	2415	0050	1720	0200	2715	0150	2020	0200	2695	0050	2130	0100	2700	0100	1945	0050	2945	0050	2365	0150
1817	0189	2427	0173	1790	0326	2723	0177	2023	0170	2700	0061	2130	0081	2700	0061	1947	0059	2987	0067	2363	0176
1810	0200	2425	0150	1740	0202	2725	0150	2020	0163	2698	0082	2126	0082	2770	0082	1945	0050	2920	0043	2368	0129
1816	0215	2426	0141	1740	0252	2710	0194	2020	0209	2696	0084	2132	0117	2700	0089	1950	0109	2930	0063	2362	0163
1820	0216	2428	014	1743	0244	2713	0075	2013	0244	2698	0125	2132	0107	2705	0138	1957	0108	2933	0100	2360	0124
1823	0213	2430	0150	1743	0225	2710	0207	2010	0239	2693	0117	2134	0202	2706	0133	1961	0204	2936	0104	2364	0177
1814	0226	2410	0122	1793	0210	2715	0234	2014	0244	2693	0108	2133	0119	2704	0131	1959	0202	2935	0100	2370	0223
1818	0216	2420	0151	1792	0199	2714	0223	2016	0236	2694	0119	2132	0116	2703	0127	1957	0201	2936	0101	2369	0214
1817	0206	2424	0170	1792	0190	2716	0217	2015	0224	2694	0112	2134	0124	2704	0123	1961	0231	2937	0104	2369	0202
1870	0000	2600	0000	1830	0000	2550	0000	2100	0000	2870	0100	2210	0000	3070	0000	2110	0000	3250	0000	2930	0000
1865	0050	2570	0300	1805	0250	2945	0050	2125	0250	2900	0300	2240	0300	3065	0050	2080	0300	3235	0150	2920	0100
1857	0123	2563	0262	1800	0216	2953	0125	2133	0238	2907	0264	2237	0249	3077	0129	2077	0254	3240	0141	2930	0163
1860	0122	2575	0304	1808	0227	2953	0103	2126	0227	2900	0174	2230	0144	3080	0122	2085	0253	3245	0150	2933	0147
1858	0122	2568	0306	1802	0232	2952	0100	2132	0223	2901	0243	2236	0252	3078	0123	2078	0273	3240	0167	2932	0133
1857	0113	2573	0305	1808	0256	2952	0098	2130	0208	2908	0255	2233	0235	3065	0109	2085	0292	3242	0152	2932	0183
1864	0216	2577	0297	1807	0239	2957	0118	2126	0222	2907	0238	2239	0254	3073	0260	2089	0266	3241	0148	2927	0198
1861	0214	2576	0278	1806	0223	2951	0169	2130	0234	2905	0223	2241	0247	3079	0269	2091	0275	3241	0136	2937	0198
1864	0223	2560	0272	1809	0224	2950	0163	2126	0256	2904	0218	2240	0235	3068	0250	2094	0276	3242	0135	2934	0150
1863	0216	2581	0270	1811	0222	2950	0154	2126	0243	2905	0206	2236	0254	3080	0262	2095	0261	3245	0150	2936	0134
1890	0000	2700	0000	1870	0000	3130	0000	2210	0000	3050	0000	2300	0000	3310	0000	2200	0000	3500	0000	2660	0000
1910	0200	2605	0150	1845	0290	3120	0100	2195	0150	3060	0200	2330	0300	3320	0100	2190	0100	3450	0200	2675	0259
1917	0191	2693	0177	1850	0216	3123	0100	2193	0130	3070	0182	2327	0249	3320	0081	2197	0133	3483	0173	2650	0216
1920	0173	2603	0178	1860	0254	3123	0082	2196	0129	3063	0126	2335	0259	3320	0070	2190	0156	3480	0156	2675	0206
1914	0196	2604	0179	1844	0242	3126	0136	2204	0176	3078	0257	2336	0237	3314	0139	2160	0153	3458	0147	2652	0216
1918	0203	2605	0160	1842	0228	3123	0161	2200	0182	3061	0273	2338	0234	3317	0137	2160	0161	3468	0161	2637	0213
1920	0192	2603	0157	1840	0213	3123	0151	2203	0184	3083	0272	2337	0220	3316	0134	2167	0152	3477	0152	2631	0211
1923	0192	2606	0172	1843	0210	3123	0139	2200	0177	3080	0261	2336	0205	3319	0165	2193	0198	3479	0165	2631	0212
1923	0163	2604	0171	1840	0210	3121	0139	2200	0176	3063	0268	2339	0208	3321	0153	2191	0163	3476	0167	2639	0213
1925	0180																				

LOG HEADING	ACC PRT	SR 1	SR 2	SR 3	SR 4	SR 5	SR 6	SR 7	SR 8	MNR 1	RR 2	TC01	TC02	TC03	TC04	TC05	TC06			
MWD	MWD	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	PER	PER	FAR	FAR	FAR	FAR	MID	MID			
10-1	10-1	F	F	F	F	F	F	F	F	CENT	CENT	HOT	COLD	HOT	COLD	HOT	COLD			
SE13 BA T 1206 0029 0030		0032 0033 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049	COME	COME	SR 1	SR 2	SR 3	SR 4	SR 5	SR 6	SR 7	SR 8	MNR 1	RR 2	TC01	TC02	TC03	TC04	TC05	TC06
SE13 BA T 1206 727 0547		0134 0160 3027 3028 3029 3028 3029 3030 3028 0079 0080 0080 0227 0141 0270 0164 0320 0227	IMLT	OUTL	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	HTIN	PER	PER	FAR	FAR	FAR	FAR	MID	MID
SE13 BA T 1207 727 0600		0133 0160 3027 3028 3029 3028 3029 3030 3028 0079 0080 0080 0225 0142 0272 0165 0321 0225																		
SE13 BA T 1208 727 0549		0133 0161 3027 3027 3028 3027 3028 3029 3030 0079 0080 0080 0223 0144 0271 0153 0317 0223																		
SE13 BA T 1209 727 0600		0133 0161 3027 3027 3028 3026 3026 3029 3030 0079 0080 0080 0221 0143 0272 0152 0316 0221																		
SE13 BA T 1210 727 0540		0134 0160 3027 3027 3028 3026 3026 3028 3029 0079 0080 0080 0220 0145 0273 0151 0314 0220																		
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 7 1.25 -1.11 27.0 0254 1853 0227 3195 0206 2243 0248 3158 0173 2390 0273 3415 0206 2228 0341 3568 0172 2668 0194  
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LOG HEADING ACC PWRT  
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 F F 10-2 10-2 10-2 10-2 10-2 10-2 10-2 10-2 CENT CENT HOT COLD HOT COLD HOT COLD  
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TC07 TC08 TC09 TC10 TC11 TC12 TC1 TC14 TC15 HT 1 HT-1 HT-1 TC01 TC01 TC02 TC03 TC04 TC05 TC06 TC07 TC08 TC09 TC00 TC04 TC05 TC07 TC08 TC09 TC00  
HTD HTD HEAT MEAN MEAN MEAN FAT EXT FAT BOLT OUTL FLOW AVG SIGN AVG  
HTD COLD OUT COLD HOT COLD MEAN BOY FAM TDM TEMP 1 1 10 2 1 1 10 1 10 2 10 2 10 1 10 2 10 1 10 2 10 1 10 2 10 1 10 2 10 1 10 2 10 1

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LOG HEADING	ACC PWRT	MWD MW	10-1 1C-1	CORE 1	CORE 2	SR 1	SR 2	SR 3	SR 4	SR 5	SR 6	SR 7	SR 8	RR 1	RR 2	TC01	TC02	TC03	TC04	TC05	TC06	TC07
SE13 BA H 2330 0029 0030				!NLT	OUTL	HTIN	PER	PER	FAR	FAR	FAR	MID	MID	MID								
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 123 0838 0277 0814 0146 0855 0253 0824 0290 0852 0233 0842 0221 0875 0250 0828 0321 0880 0161 0834 0267  
 129 0837 0271 0815 0145 0857 0253 0824 0280 0852 0224 0839 0229 0871 0267 0826 0313 0881 0166 0836 0275  
 126 0837 0262 0816 0145 0858 0246 0825 0270 0851 0223 0836 0253 0870 0263 0827 0202 0883 0166 0838 0272  
 127 0836 0257 0817 0144 0860 0250 0825 0262 0851 0216 0834 0252 0868 0272 0826 0295 0884 0165 0841 0281  
 123 0835 0253 0819 0173 0860 0242 0825 0255 0859 0222 0833 0252 0866 0268 0827 0293 0885 0172 0841 0274  
 125 0834 0247 0820 0169 0862 0246 0825 0247 0843 0221 0832 0250 0864 0273 0826 0291 0886 0171 0843 0281  
 122 0833 0243 0818 0189 0859 0256 0824 0247 0849 0219 0834 0267 0865 0268 0823 0263 0884 0184 0841 0290  
 118 0834 0244 0818 0183 0858 0258 0822 0252 0848 0223 0835 0261 0867 0272 0828 0301 0885 0188 0841 0283

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LOG HEADING	ACC	PWRT	SR	CORE	CORE	SR	SR	SR	SR	SR	SR	RR	RR	RR	TCO1	TCO2	TCO3	TCO4	TCO5	TCO6	TCO7	
	MWD	MW	INTL	OUTL	HTIN	PER	FET	FAR	FAR	FAR	FAR	MID	MID	MID	MID							
10-1	10-1		F	F	10-2	10-2	10-2	10-2	10-2	10-2	10-2	10-2	10-2	CENT	CENT	HOT	COLD HOT	COLD HOT	COLD HOT	COLD HOT		
SE14 BA H	0530	0029	0030	0032	0033	0034	0035	0036	0037	0038	0039	0040	0041	0042	0043	0044	0045	0046	0047	0048	0049	0050
SE14 BA T	0530	7510	0012	0068	0068	0001	0005	-002	-004	-070	0006	0001	0004	0002	-001	0077	0076	0078	0079	0082	0080	0082
SE14 EA T	0531	7510	0013	0068	0068	0001	0003	-002	-004	-070	0006	0001	0004	0002	-001	0075	0078	0081	0081	0082	0080	0079
SE14 BA T	0532	7510	0012	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0078	0076	0078	0077	0083	0082	0082
SE14 BA T	0533	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0075	0077	0080	0081	0082	0080	0079
SE14 BA T	0534	7510	0013	0068	0068	0001	0003	-002	-004	-070	0006	0001	0004	0002	-001	0081	0083	0081	0077	0078	0075	0079
SE14 BA T	0535	7510	0013	0068	0068	0001	0003	-002	-004	-070	0006	0001	0004	0002	-001	0077	0076	0078	0077	0082	0081	0082
SE14 BA T	0536	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0081	0083	0081	0077	0078	0075	0078
SE14 BA T	0537	7510	0013	0068	0068	0001	0003	-002	-004	-070	0006	0001	0004	0002	-001	0081	0079	0076	0075	0080	0081	0083
SE14 BA T	0538	7510	0012	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0077	0076	0078	0077	0082	0081	0082
SE14 BA T	0539	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0081	0083	0081	0077	0078	0075	0078
SE14 BA T	0540	7510	0012	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0081	0079	0076	0075	0081	0081	0082
SE14 BA T	0541	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0003	0002	-001	0077	0076	0078	0077	0082	0081	0082
SE14 BA T	0542	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0082	0082	0082	0082	0083	0080	0080
SE14 BA T	0543	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0077	0077	0079	0081	0081	0081	0081
SE14 BA T	0544	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0082	0076	0077	0079	0083	0080	0080
SE14 BA T	0545	7510	0012	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0077	0081	0081	0079	0081	0076	0077
SE14 BA T	0546	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0004	0002	-001	0079	0077	0077	0075	0081	0081	0081
SE14 BA T	0547	7510	0013	0068	0068	0000	0004	002	-004	-070	0006	0001	0003	0002	-001	0076	0082	0081	0079	0082	0075	0077
SE14 BA T	0548	7510	0012	0068	0068	0001	0005	002	-004	-070	0006	0001	0004	0002	-001	0076	0077	0081	0080	0081	0077	0078
SE14 BA T	0549	7510	0013	0068	0068	0000	0003	-002	-004	-070	0006	0001	0003	0002	-001	0077	0081	0081	0079	0081	0076	0077



**BLANK PAGE**

TC02	TC03	TC03	TC04	TC04	TC05	TC05	TC06	TC06	TC07	TC07	T <sub>07-08</sub>	TC08	TC09	TC09	TC10	TC10	TC11	TC11	TC12	TC12
134	Avg	SIGM	Avg	SIGM	Avg	SIGM	Avg	SIGM	Avg	SIGM	Avg	SIGM								
5-2	10-1	10-2	10-1	10-2	1u	1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1	10-2	10-1
065	0066	0067	0068	0069	0070	0071	0072	0073	0074	0075	0076	0077	0078	0079	0080	0081	0082	0083	0084	0085
000	0780	0000	0790	0000	0820	0000	0800	0000	0820	0000	0770	0000	0800	0000	0770	0000	0830	0000	0820	0000
100	0795	0150	0000	0100	0820	0000	0800	0000	0805	0150	0760	0100	0805	0050	0765	0150	0845	0150	0820	0000
200	0795	0141	0790	0163	0823	0050	0807	0101	0810	0141	0767	0125	0800	0061	0777	0174	0833	0211	0817	0068
300	0793	0129	0795	0165	0823	0043	0805	0086	0805	0150	0763	0129	0800	0070	0760	0158	0840	0212	0818	0043
400	0796	0138	0790	0178	0814	0177	0794	0234	0802	0149	0772	0223	0812	0251	0786	0188	0836	0208	0808	0197
500	0793	0138	0787	0162	0815	0164	0797	0221	0805	0150	0773	0208	0808	0241	0782	0193	0835	0189	0808	0177
600	0796	0140	0784	0178	0810	0192	0790	0261	0801	0167	0779	0230	0814	0269	0786	0207	0833	0183	0803	0172
700	0791	0176	0780	0200	0808	0192	0791	0247	0805	0180	0783	0238	0814	0249	0783	0210	0831	0176	0799	0226
800	0788	0194	0777	0211	0808	0181	0793	0240	0807	0177	0786	0241	0813	0236	0779	0225	0829	0180	0790	0217
900	0786	0198	0776	0203	0809	0175	0795	0233	0808	0178	0785	0229	0811	0235	0777	0220	0828	0173	0800	0214
1000	0785	0185	0773	0219	0807	0178	0793	0231	0809	0169	0788	0242	0813	0231	0776	0211	0823	0161	0796	0235
1100	0784	0181	0774	0214	0809	0181	0793	0225	0808	0162	0786	0243	0812	0223	0778	0206	0828	0167	0798	0227
1200	0786	0187	0775	0209	0809	0173	0791	0234	0805	0188	0785	0237	0812	0215	0778	0232	0828	0161	0798	0221
1300	0785	0184	0774	0213	0809	0167	0792	0231	0808	0181	0786	0232	0811	0211	0776	0236	0826	0160	0799	0216
1400	0787	0199	0775	0210	0809	0164	0790	0236	0805	0179	0785	0227	0810	0209	0779	0241	0828	0164	0800	0220
1500	0787	0198	0773	0219	0807	0172	0788	0240	0806	0176	0787	0236	0811	0206	0779	0238	0827	0162	0798	0215
1600	0786	0131	0771	0226	0805	0178	0788	0234	0806	0175	0788	0236	0812	0204	0778	0228	0825	0169	0796	0220
1700	0787	0194	0772	0225	0806	0178	0786	0243	0804	0190	0787	0233	0813	0202	0779	0224	0827	0191	0797	0223
1800	0788	0196	0773	0227	0806	0173	0785	0239	0803	0193	0786	0235	0812	0199	0781	0226	0826	0200	0797	0220

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 Astronuclear  
Laboratory  
WANL-TME-1710  
November, 1967

APPENDIX B

Program To Reduce Data

Attached is the IBM compilation of the computer program written to reduce the temperature data to heating rates and to record all other data associated with the calorimeter measurements.



000241 280 FORMAT (6F17.3//) /  
000241 290 WHITE (6.270)  
000245 300 WHITE (6.280) MNER. FMID. MFARNO  
000265 120 GO TO 20  
000266 FNR

1

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150	1511	-	377.51151.0155.155	WET, WNW	0.022201 - 0.51/4
151	1511	-	372.51160.1150.155	WET, WNW	0.022201 - 0.51/4
152	1511	-	367.51161.0150.155	WET, WNW	0.022201 - 0.51/4
153	1511	-	362.51161.0150.155	WET, WNW	0.022201 - 0.51/4
154	1511	-	357.51151.0155.155	WET, WNW	0.022201 - 0.51/4
155	1511	-	352.51126.0130.135	WET, WNW	0.022201 - 0.51/4
156	1511	-	347.51121.0125.125	WET, WNW	0.022201 - 0.51/4
157	1511	-	342.51116.0120.120	WET, WNW	0.022201 - 0.51/4
158	1511	-	340.51111.0115.115	WET, WNW	0.022201 - 0.51/4
159	1511	-	337.51111.0115.115	WET, WNW	0.022201 - 0.51/4
160	1511	-	332.51106.0110.110	WET, WNW	0.022201 - 0.51/4
161	1511	-	327.51101.0105.105	WET, WNW	0.022201 - 0.51/4
162	1511	-	322.5.40.100.100	WET, WNW	0.022201 - 0.51/4
163	1511	-	317.51.91.0.91.0	WET, WNW	0.022201 - 0.51/4
164	1511	-	312.51.46.0.90.90	WET, WNW	0.022201 - 0.51/4
165	1511	-	307.51.41.0.91.0	WET, WNW	0.022201 - 0.51/4
166	1511	-	302.51.36.0.91.0	WET, WNW	0.022201 - 0.51/4
167	1511	-	297.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
168	1511	-	292.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
169	1511	-	287.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
170	1511	-	282.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
171	1511	-	277.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
172	1511	-	272.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
173	1511	-	267.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
174	1511	-	262.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
175	1511	-	257.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
176	1511	-	252.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
177	1511	-	247.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
178	1511	-	242.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
179	1511	-	237.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
180	1511	-	232.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
181	1511	-	227.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
182	1511	-	222.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
183	1511	-	217.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
184	1511	-	212.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
185	1511	-	207.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
186	1511	-	202.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
187	1511	-	197.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
188	1511	-	192.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
189	1511	-	187.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
190	1511	-	182.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
191	1511	-	177.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
192	1511	-	172.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
193	1511	-	167.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
194	1511	-	162.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
195	1511	-	157.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
196	1511	-	152.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
197	1511	-	147.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
198	1511	-	142.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
199	1511	-	137.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
200	1511	-	132.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
201	1511	-	127.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
202	1511	-	122.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
203	1511	-	117.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
204	1511	-	112.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
205	1511	-	107.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
206	1511	-	102.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
207	1511	-	97.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
208	1511	-	92.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
209	1511	-	87.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
210	1511	-	82.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
211	1511	-	77.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
212	1511	-	72.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
213	1511	-	67.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
214	1511	-	62.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
215	1511	-	57.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
216	1511	-	52.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
217	1511	-	47.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
218	1511	-	42.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
219	1511	-	37.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
220	1511	-	32.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
221	1511	-	27.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
222	1511	-	22.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
223	1511	-	17.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
224	1511	-	12.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
225	1511	-	7.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
226	1511	-	2.5111.0.91.0	WET, WNW	0.022201 - 0.51/4
227	1511	-	0.5111.0.91.0	WET, WNW	0.022201 - 0.51/4

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900 SUBROUTINE CUP(LCT, ITCM1, ITCM2, ITCM3, ITCM4, ITCM5, ITCM6, ITCM7, ITCM8).
1 ITCM2, ITCM10, ITCM11, ITCM12)
100 IF (I4 - 1) 105, 105, 200
105 IF (I6 - 2, 4, 2) 106, 110, 110
106 TCR1 = 1.00*(123.16484 • 3.31) • 32.0
108 RETURN
110 IF (I6 - 5, 52) 111, 115, 115
111 ICH1 = 1.00*(123.43484 • 2.54) • 32.0
112 ICH2 = 1.00*(125.57104 - 7.15) • 32.0
113 ICH3 = 1.00*(125.18064 - 6.99) • 32.0
114 ICH4 = 1.00*(125.18064 - 6.99) • 32.0
115 ICH5 = 1.00*(125.18064 - 6.99) • 32.0
116 ICH6 = 1.00*(125.18064 - 6.99) • 32.0
117 ICH7 = 1.00*(125.18064 - 6.99) • 32.0
118 ICH8 = 1.00*(125.18064 - 6.99) • 32.0
119 ICH9 = 1.00*(125.18064 - 6.99) • 32.0
120 IF (I6 - 6, 16) 121, 125, 125
121 TCR1 = 1.00*(125.57104 - 10.15) • 32.0
122 RETURN
123 IF (I6 - 10, 33) 126, 130, 130
124 TCR1 = 1.00*(125.57104 - 10.15) • 32.0
125 IF (I6 - 10, 33) 131, 135, 135
126 TCR1 = 1.00*(125.57104 - 10.15) • 32.0
127 MRETURN
128 IF (I6 - 6, 9) 129, 136, 136
129 MRETURN
130 IF (I6 - 12, 38) 131, 135, 135
131 TCR1 = 1.00*(123.43484 • 12.13) • 32.0
132 MRETURN
133 IF (I6 - 13, 23) 134, 136, 136
134 TCR1 = 1.00*(126.70603 - 6.98) • 32.0
135 IF (I6 - 14, 59) 141, 145, 145
136 TCR1 = 1.00*(123.52603 - 11.71) • 32.0
137 MRETURN
138 IF (I6 - 15, 84) 139, 140, 140
139 TCR1 = 1.00*(123.52603 - 11.71) • 32.0
140 IF (I6 - 16, 99) 141, 145, 145
141 TCR1 = 1.00*(123.52603 - 11.71) • 32.0
142 MRETURN
143 IF (I6 - 17, 114) 144, 148, 148
144 TCR1 = 1.00*(123.70603 - 6.98) • 32.0
145 IF (I6 - 18, 121) 211, 215, 215
146 TCR1 = 1.00*(123.70603 - 6.98) • 32.0
147 MRETURN
148 IF (I6 - 19, 124) 205, 205, 300
149 IF (I6 - 20, 124) 206, 210, 210
150 TCR2 = 1.00*(23.23284 • 2.07) • 32.0
151 MRETURN
152 IF (I6 - 21, 125) 216, 220, 220
153 TCR2 = 1.00*(24.47104 - 1.70) • 32.0
154 MRETURN
155 IF (I6 - 22, 125) 221, 225, 225
156 TCR2 = 1.00*(25.47204 - 0.09) • 32.0
157 MRETURN
158 IF (I6 - 23, 125) 226, 230, 230
159 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
160 MRETURN
161 IF (I6 - 24, 125) 231, 235, 235
162 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
163 MRETURN
164 IF (I6 - 25, 125) 236, 240, 240
165 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
166 MRETURN
167 IF (I6 - 26, 125) 241, 245, 245
168 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
169 MRETURN
170 IF (I6 - 27, 125) 246, 250, 250
171 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
172 MRETURN
173 IF (I6 - 28, 125) 251, 255, 255
174 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
175 MRETURN
176 IF (I6 - 29, 125) 256, 260, 260
177 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
178 MRETURN
179 IF (I6 - 30, 125) 261, 265, 265
180 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
181 MRETURN
182 IF (I6 - 31, 125) 266, 270, 270
183 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
184 MRETURN
185 IF (I6 - 32, 125) 271, 275, 275
186 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
187 MRETURN
188 IF (I6 - 33, 125) 276, 280, 280
189 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
190 MRETURN
191 IF (I6 - 34, 125) 281, 285, 285
192 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
193 MRETURN
194 IF (I6 - 35, 125) 286, 290, 290
195 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
196 MRETURN
197 IF (I6 - 36, 125) 291, 295, 295
198 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
199 MRETURN
200 IF (I6 - 37, 125) 296, 300, 300
201 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
202 MRETURN
203 IF (I6 - 38, 125) 301, 305, 305
204 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
205 MRETURN
206 IF (I6 - 39, 125) 306, 310, 310
207 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
208 MRETURN
209 IF (I6 - 40, 125) 311, 315, 315
210 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
211 MRETURN
212 IF (I6 - 41, 125) 316, 320, 320
213 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
214 MRETURN
215 IF (I6 - 42, 125) 321, 325, 325
216 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
217 MRETURN
218 IF (I6 - 43, 125) 326, 330, 330
219 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
220 MRETURN
221 IF (I6 - 44, 125) 331, 335, 335
222 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
223 MRETURN
224 IF (I6 - 45, 125) 336, 340, 340
225 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
226 MRETURN
227 IF (I6 - 46, 125) 341, 345, 345
228 TCR2 = 1.00*(24.34104 • 0.43) • 32.0
229 MRETURN
230 IF (I6 - 47, 125) 346, 350, 350
231 MRETURN
232 IF (I6 - 48, 125) 351, 355, 355
233 MRETURN

```

000203	231	TC62	= 1.0e(25.0660E - 23.66) + 32.0
000210	235	1E - 12.00E 236.00E 240.0	24n
000210	236	1C62 = 1.0e(25.0770E + 16.23) + 32.0	
000220	240	IF 1E - 13.53E 241.0205E 245.	
000223	241	1C62 = 1.0e(25.0280E - 4.42) + 32.0	
000230	245	1E - 14.67E 246.0250E 25n	
000230	246	1C62 = 1.0e(25.0930E + 34.24) + 32.0	
000240	250	RETURN	
000240	250	1C62 = 1.0e(23.0850E + 4.64) + 32.0	
000245	260	IF IN - 31.305. 305. 400	
000247	305	IF 1E - 2.27E 306.310. 310. 311. + 32.0	
000252	306	1C63 = 1.0e(23.0850E - 1.31) + 32.0	
000257	310	IF 1E - 3.13E 311.315. 315. 316. + 32.0	
000262	311	1C63 = 1.0e(25.07440E - 8.71) + 32.0	
000267	315	IF 1E - 4.00E 316.320. 320. 321. + 32.0	
000267	316	1C63 = 1.0e(25.0750E + 6.53) + 32.0	
000272	316	IF 1E - 5.00E 316.320. 320. 321. + 32.0	
000277	320	IF 1E - 6.077E 321.325. 325. 326. + 32.0	
000302	321	1C63 = 1.0e(25.04390E - 8.04) + 32.0	
000307	325	IF 1E - 6.085E 326.330. 330. 331. + 32.0	
000312	326	1C63 = 1.0e(25.09170E + 8.02) + 32.0	
000317	326	IF 1E - 9.050E 331.335. 335. 336. + 32.0	
000322	331	1C63 = 1.0e(25.04060E - 5.61) + 32.0	
000327	335	IF 1E - 10.05E 336.340. 340. 341. + 32.0	
000327	336	1C63 = 1.0e(25.02170E - 8.57) + 32.0	
000332	340	IF 1E - 12.30E 341.345. 345. 346. + 32.0	
000337	341	1C63 = 1.0e(25.02740E + 1.45) + 32.0	
000342	345	IF 1E - 12.30E 341.345. 345. 346. + 32.0	
000347	345	1C63 = 1.0e(25.01240E + 4.56) + 32.0	
000354	400	IF IN - 6.000. 405. 500.	
000356	405	IF 1E - 4.00E 410. 410. 410. + 32.0	
000361	406	1C63 = 1.0e(25.0160E + 4.16) + 32.0	
000366	410	IF 1E - 6.013E 411.415. 415. 416. + 32.0	
000371	411	1C63 = 1.0e(25.03460E - 2.71) + 32.0	
000376	411	IF 1E - 6.013E 411.415. 415. 416. + 32.0	

8

```

000376 415 IF (E -11.66) 416, 420, 420, 420
000401 416 TCR4 = 1.8e(23.715e0 E . 0.48) + 32.0
000406 420 IF (E -13.45) 421, 425, 425
000411 421 TCR4 = 1.8e(22.905e0 E . 17.93) + 32.0
000415 425 IF (E -14.57) 426, 430, 430
000421 426 TCR4 = 1.8e(24.107e0 E . 1.76) + 32.0
000426 430 IF (E -16.66) 431, 435, 435
000431 431 TCR4 = 1.8e(22.967e0 E . 18.38) + 32.0
000436 435 IF (E -18.02) 436, 440, 440
000441 436 TCR4 = 1.8e(25.735e0 E - 27.75) + 32.0
000446 440 RETURN
000451 441 IF (E -19.15) 441, 445, 445
000456 441 TCR4 = 1.8e(23.894e0 E . 5.43) + 32.0
000459 445 IF (E -20.24) 446, 450, 450
000461 446 TCR4 = 1.8e(22.011e0 E . 41.35) + 32.0
000466 450 RETURN
000466 450 TCR4 = 1.8e(20.455e0 E + 73.00) + 32.0
000473 500 IF (N - 5) 505, 505, 600
000475 505 IF (E - 2.27) 506, 510, 510
000500 506 TC5 = 1.8e(24.031e0 E - 2.55) + 32.0
000505 510 RETURN
000506 510 IF (E - 3.12) 511, 515, 515
000511 511 TC5 = 1.8e(27.059e0 E - 9.42) + 32.0
000516 515 IF (E - 4.07) 516, 520, 520
000522 516 TCR5 = 1.8e(22.105e0 E . 6.03) + 32.0
000527 520 IF (E - 7.03) 521, 525, 525
000530 521 TCR5 = 1.8e(23.311e0 E . 1.13) + 32.0
000533 525 RETURN
000540 525 IF (E - 9.71) 526, 530, 530
000541 526 TCR5 = 1.8e(24.627e0 E - 8.13) + 32.0
000551 530 IF (E -10.95) 531, 535, 535
000552 531 TCR5 = 1.8e(24.387e0 E . 3.91) + 32.0
000555 535 IF (E -12.75) 536, 540, 540
000562 536 TCR5 = 1.8e(23.333e0 E . 4.51) + 32.0
000563 540 RETURN
000566 540 TC5 = 1.8e(24.104e0 E - 5.33) + 32.0
000573 540 RETURN
000574 540 TC5 = 1.8e(24.104e0 E - 5.33) + 32.0
000601 540 RETURN

```

```

000602    600    IF (N = 6) 605, 605, 700
000604    605    IF (E = 2.2E) 610, 610, 610
000607    606    1C6 = 1.0*(24.031*E - 2.79) + 32.0
000614    MRETURN
000615    610    IF (E = 3.12) 611, 615, 615
000620    611    1CH6 = 1.0*(27.381*E - 10.43) + 32.0
000625    MRETURN
000626    615    IF (E = 4.00) 616, 620, 620
000631    616    TCR6 = 1.0*(21.875*E + 6.75) + 32.0
000636    MRETURN
000637    620    IF (E = 7.00) 621, 625, 625
000642    621    TCR6 = 1.0*(23.637*E - 0.41) + 32.0
000647    MRETURN
000650    625    IF (E = 9.73) 626, 630, 630
000653    626    1CH6 = 1.0*(24.176*E - 4.23) + 32.0
000660    MRETURN
000661    630    IF (E = 10.92) 631, 635, 635
000664    631    TCR6 = 1.0*(24.370*E - 6.12) + 32.0
000671    MRETURN
000672    635    IF (E = 12.75) 636, 640, 640
000675    636    1CH6 = 1.0*(22.951*E + 9.38) + 32.0
000702    MRETURN
000703    640    TCR6 = 1.0*(24.503*E - 10.47) + 32.0
000710    MRETURN
000711    700    IF (N = 7) 705, 705, 800
000713    705    IF (E = 4.61) 706, 710, 710
000716    706    TCR7 = 1.0*(22.606*E + 5.78) + 32.0
000723    MRETURN
000724    710    IF (E = 9.23) 711, 715, 715
000727    711    TCR7 = 1.0*(24.892*E - 4.75) + 32.0
000734    MRETURN
000735    715    IF (E = 10.13) 716, 720, 720
000740    716    TCR7 = 1.0*(24.444*E - 0.62) + 32.0
000745    MRETURN
000746    720    IF (E = 11.65) 721, 725, 725
000751    721    TCR7 = 1.0*(25.000*E - 6.25) + 32.0
000756    MRETURN
000757    725    IF (E = 13.38) 726, 730, 730
000762    726    TCR7 = 1.0*(23.699*E + 8.90) + 32.0
000767    MRETURN
000770    730    IF (E = 14.52) 731, 735, 735
000773    731    TCR7 = 1.0*(23.684*E + 9.11) + 32.0
001000    MRETURN
001001    735    IF (E = 16.61) 736, 740, 740
001004    736    TCR7 = 1.0*(22.967*E + 19.53) + 32.0
001011    MRETURN
001012    740    IF (E = 18.14) 741, 745, 745

```

001015	741	TC47 = 1.**(22.075** + 21.01) + 32.0
001022		MF1UHN
001023	745	IF (E - 19.22) 146.750 + 750
001026	746	TC47 = 1.**(25.000** - 17.50) + 32.0
001033		MF1UHN
001034	750	IF (E - 20.26) 751.755 + 755
001037	751	TC47 = 1.**(23.077** + 19.46) + 32.0
001044		MF1UHN
001045	755	TC47 = 1.**(24.324** - 5.81) + 32.0
001052		MF1UHN
001053	800	IF (N - 8) 805.805 + 900
001055	805	IF (L - 4.53) 806.810 + 810
001060	806	TC4H = 1.**(23.599** + 3.10) + 32.0
001065		MF1UHN
001066	810	IF (L - 9.25) 811.815 + 815
001071	811	TC4H = 1.**(24.364** - 0.31) + 32.0
001076		MF1UHN
001077	815	IF (E - 10.11) 816.820 + 820
001078	816	TC4H = 1.**(25.581** - 11.63) + 32.0
001079		MF1UHN
001100	820	IF (E - 11.44) 821.825 + 825
001107	821	TC4H = 1.**(24.837** - 4.11) + 32.0
001110		MF1UHN
001113	825	IF (E - 13.34) 826.830 + 830
001120		MF1UHN
001121	826	TC4H = 1.**(23.563** + 10.72) + 32.0
001124		MF1UHN
001131	830	IF (L - 14.54) 831.835 + 835
001132		MF1UHN
001135	831	TC4H = 1.**(23.276** + 14.57) + 32.0
001142		MF1UHN
001143	835	IF (E - 16.54) 836.840 + 840
001146		MF1UHN
001153	836	TC4H = 1.**(23.529** + 10.84) + 32.0
001154		MF1UHN
001157	840	IF (E - 18.15) 841.845 + 845
001164		MF1UHN
001165	845	IF (E - 19.16) 846.850 + 850
001170		MF1UHN
001175	846	TC4H = 1.**(23.733** - 4.92) + 32.0
001176		MF1UHN
001203	850	TC4H = 1.**(24.419** - 4.08) + 32.0
001204	900	IF (N - 9) 905.905 + 1000
001206	905	IF (E - 1.97) 906.910 + 910
001211	906	TC4H = 1.**(24.000** + 0.72) + 32.0
001216		MF1UHN
001217	910	IF (E - 2.65) 911.915 + 915
001222		MF1UHN
001227	911	IF (E - 24.615** + 0.49) + 32.0

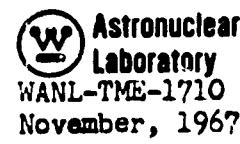
001230	915	IF (E - 3.09) 916, 920, 920,
001233	916	TC49 = 1.4*(23.1348t + 2.61) + 32.0
001240	920	IF (E - 5.49) 921, 925, 925
001241	921	TC49 = 1.4*(24.8328t - 4.08) + 32.0
001244		RETURN
001251		RETURN
001252	925	IF (E - 5.74) 926, 930, 930
001255	926	TC49 = 1.8*(25.6678t - 14.14) + 32.0
001262		RETURN
001263	930	IF (E - 8.17) 931, 935, 935
001266	931	TC49 = 1.8*(24.2688t - 0.27) + 32.0
001273	935	IF (E - 10.49) 936, 940, 940
001274	936	TC49 = 1.8*(24.2428t - 0.06) + 32.0
001277	936	RETURN
001304	940	IF (E - 12.40) 941, 945, 945
001305	941	TC49 = 1.8*(25.0008t - 8.00) + 32.0
001310		RETURN
001315	945	IF (E - 13.26) 946, 950, 950
001316	946	TC49 = 1.8*(24.1988t - 0.80) + 32.0
001321		RETURN
001326	950	IF (E - 14.62) 951, 955, 955
001327	951	TC49 = 1.8*(23.5298t + 11.01) + 32.0
001332		RETURN
001337	955	IF (E - 16.67) 956, 960, 960
001340	956	TC49 = 1.8*(22.9278t + 19.81) + 32.0
001343		RETURN
001350	960	IF (E - 14.328t + 3.05) + 32.0
001351		RETURN
001356	960	IF (E - 10.1105.1005.1015
001357		TC49 = 1.8*(23.5088t + 3.11) + 32.0
001361	1005	IF (E - 1.911106.1010.1010
001364	1006	TC49 = 1.8*(24.4588t + 0.91) + 32.0
001371		RETURN
001372	1010	IF (E - 3.0111.11.1015.1015
001375	1011	TC49 = 1.8*(23.5088t + 3.11) + 32.0
001402		RETURN
001403	1015	IF (E - 5.0411.16.1020.1020
001406	1016	TC49 = 1.8*(24.0778t + 4.77) + 32.0
001413		RETURN
001414	1020	IF (E - 9.4211.21.1025.1025
001417	1021	TC49 = 1.8*(12.4.4958t - 3.46) + 32.0
001424		RETURN
001426	1025	IF (E - 12.4311.29.1030.1030
001430	1026	TC49 = 1.8*(12.4.4118t - 7.63) + 32.0
001435		RETURN
001436	1030	IF (E - 13.3111031.1035.1035
001461	1031	TC49 = 1.8*(12.3.6848t + 7.81) + 32.0

001446	001447	1035	IF (E - 1.453)1036.01040.1040	NETUWN
001452	1036	TC410 = 1.00(22.0002 + 10.85) + 32.0	NETUWN	
001457	1040	IF (E - 15.56)1041.1045.1045	NETUWN	
001460	1041	TC410 = 1.00(129.1760E - 0.69) + 32.0	NETUWN	
001463	1045	TC410 = 1.00(22.9810E + 19.43) + 32.0	NETUWN	
001470	1100	IF (N - 1111105.1105.1205	NETUWN	
001471	1105	IF (E - 1.62)1106.1110.1110	NETUWN	
001476	1106	TC411 = 1.00(24.6580E + 0.66) + 32.0	NETUWN	
001477	1110	IF (E - 3.92)1111.1115.1115	NETUWN	
001501	1111	TC411 = 1.00(25.5000E + 2.99) + 32.0	NETUWN	
001504	1115	IF (E - 5.91)1116.1120.1120	NETUWN	
001511	1116	TC411 = 1.00(23.8100E + 1.66) + 32.0	NETUWN	
001512	1120	IF (E - 9.85)1121.1125.1125	NETUWN	
001515	1121	TC411 = 1.00(24.0100E + 0.50) + 32.0	NETUWN	
001522	1125	IF (E - 12.63)1126.1130.1130	NETUWN	
001523	1126	TC411 = 1.00(25.1800E - 11.92) + 32.0	NETUWN	
001526	1130	IF (E - 13.02)1131.1135.1135	NETUWN	
001533	1131	TC411 = 1.00(23.0770E + 15.56) + 32.0	NETUWN	
001534	1135	IF (E - 14.63)1136.01190.01140	NETUWN	
001537	1136	TC411 = 1.00(22.9810E + 16.79) + 32.0	NETUWN	
001544	1140	IF (E - 15.56)1141.1145.1145	NETUWN	
001545	1141	TC411 = 1.00(23.6560E + 6.91) + 32.0	NETUWN	
001550	1145	IF (E - 17.3.6840E + 6.44) + 32.0	NETUWN	
001555	1150	IF (E - 2.06)1206.1210.1210	NETUWN	
001556	1206	TC412 = 1.00(24.5280E - 1.52) + 32.0	NETUWN	
001561	1207	IF (E - 4.20)1211.1215.1215	NETUWN	
001566	1210	TC412 = 1.00(24.7600E - 2.02) + 32.0	NETUWN	
001567	1211	IF (E - 5.45)1216.1220.1220	NETUWN	
001572	1215	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	
001577	1216	IF (E - 7.25)1221.1225.1225	NETUWN	
001600	1220	TC412 = 1.00(24.2860E + 0.51) + 32.0	NETUWN	
001603	1221	IF (E - 9.0)1222.1226.1226	NETUWN	
001610	1225	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	
001611	1226	IF (E - 10.75)1227.1231.1231	NETUWN	
001616	1227	TC412 = 1.00(24.2860E + 0.51) + 32.0	NETUWN	
001617	1228	IF (E - 12.5)1228.1232.1232	NETUWN	
001622	1229	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	
001627	1230	IF (E - 14.25)1233.1237.1237	NETUWN	
001630	1231	TC412 = 1.00(24.2860E + 0.51) + 32.0	NETUWN	
001633	1235	IF (E - 16.0)1238.1242.1242	NETUWN	
001640	1240	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	
001641	1245	IF (E - 17.75)1243.1247.1247	NETUWN	
001644	1246	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	
001651	1250	IF (E - 19.5)1251.1255.1255	NETUWN	
001652	1255	TC412 = 1.00(24.2860E + 0.51) + 32.0	NETUWN	
001655	1259	IF (E - 21.25)1256.1260.1260	NETUWN	
	1261	TC412 = 1.00(24.5710E - 1.20) + 32.0	NETUWN	

001662	1225	IF (t = -12.70) 1226 1230 1236	• 32.0 n
001663	1226	1C612 = 1.0e(124.8628t - 3.70)	• 32.0 n
001664		IF TUMN	
001673	1230	IF (t = -14.00) 1231 1235	• 32.0 n
001674	1231	1C612 = 1.0e(122.9518t + 20.69)	• 32.0 n
001677		IF TUMN	
001704	1235	IF (t = -15.22) 1236 1240 1245	• 32.0 n
001710	1236	1C612 = 1.0e(125.2038t - 10.80)	• 32.0 n
001715		IF TUMN	
001716	1240	IF (t = -17.21) 1241 1245 1246	• 32.0 n
001721	1241	1C612 = 1.0e(123.2328t + 19.10)	• 32.0 n
001726		IF TUMN	
001727	1245	TC612 = 1.0e(124.5288t - 3.13)	• 32.0 n
001734		IF TUMN	
001735		F.D.	

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```
000120    IF (DELT = 3H.52) 412. 420. 420
000123    H = DELT.0.02592
000125    RETURN
000129    420   IF (DELT = 115.6) 422. 430. 430
000130    422   H = DELT.0.02615
000132    RETURN
000135    430   IF (DELT = 192.6) 432. 440. 440
000136    432   H = DELT.0.02596
000137    440   IF (DELT = 231.1) 442. 452. 452
000138    442   H = DELT.0.02581
000140    452   H = DELT.0.02611
000144    RETURN
000146    END
```



### APPENDIX C

#### Reduced Data

Attached is the output of the program given in APPENDIX B. This lists all data from data logger printout (except standard deviation) and all data taken by Plum Brook WANL Test Operations personnel for the entire test.



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Fig. 1. - Cross section of a cylinder having three cylindrical faces.

RECORDED AT 10000 HZ, 16 BIT, 44.1 KHZ SAMPLING RATE, 10000 HZ NORMALIZED TO AD NY EAS CONDENSER

Consequently, the results of the present study indicate that the relationship between the two variables is not as strong as it was in the previous studies.

156.20  
156.00  
155.80  
155.60  
155.40  
155.20

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9/ 5/67. TIME = 11.03 TO 11.32 54.8 MM. 20.25 INCHES FROM FULL IN. 510 MICRONS, RDN BNK POS = 21.45 IN.  
 P11 T2=0 = 133.0 DEG F. MT1FLW = 129.8 F. MTOUTL = 129.5 F. MT1 FLOW = 61.8 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 DATA 168 TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA 169 TEMP 138.90 142.50 134.00 137.10 136.80 136.70 138.20 136.80 138.30 137.10 138.90 139.00  
 CORRECTED TEMP 138.13 139.52 132.08 139.06 131.94 129.14 139.50 137.58 136.95 137.67 138.81 135.56  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM)  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* -0.022 -0.096 -0.024 -0.024  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM)  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* -0.022 -0.096 -0.024 -0.024

9/ 5/67. TIME = 11.58 TO 11.09 54.8 MM. 20.25 INCHES FROM FULL IN. 510 MICRONS, RDN BNK POS = 21.45 IN.  
 P11 T2=0 = 133.0 DEG F. MT1FLW = 129.3 F. MTOUTL = 139.0 F. MT1 FLOW = 63.7 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 DATA 168 TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA 169 TEMP 142.90 145.80 149.00 161.10 150.50 141.90 148.90 142.60 146.50 140.50 150.90 146.20  
 CORRECTED TEMP 141.94 142.76 143.15 142.88 145.03 135.03 149.52 143.24 145.31 140.78 150.48 145.00  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM)  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* -0.022 -0.024 -0.024 -0.024  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM)  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* -0.022 -0.024 -0.024 -0.024

9/ 5/67. TIME = 11.21 TO 11.32 54.8 MM. 20.25 INCHES FROM FULL IN. 510 MICRONS, RDN BNK POS = 21.45 IN.  
 P11 T2=0 = 133.0 1.06 F. MT1FLW = 130.3 F. MTOUTL = 139.0 F. MT1 FLOW = 63.8 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 DATA 168 TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA 169 TEMP 150.70 152.40 166.30 166.20 170.40 151.50 169.90 154.50 165.10 147.50 174.70 165.60  
 CORRECTED TEMP 148.97 162.31 147.92 167.27 165.91 169.17 154.87 161.97 147.59 173.94 162.84  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM)  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* -0.022 -0.024 -0.024 -0.024

\*\*\*\*\* AT INDICATED POS, F. MTINLT = NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
DATA LGT TEMP 170.20 164.70 202.50 158.80 217.20 215.30 179.20 213.50 166.60 228.30 199.70  
CORRECTED TEMP 168.43 160.90 196.45 160.04 210.74 171.00 212.03 179.53 209.16 166.17 226.57 198.41

\*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.009 1.649 0.985 1.191 1.049 1.079

\*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
•39 0.375 •379 •382 •634 •411

9/ 5/67, TIME = 11.46 TO 11.57 54.8 MW, 19.25 INCHES FROM FULL IN, 510 MICRONS, ROD BNK POS = 21.48 IN.  
FIR TEMP = 135.0 DEG F. MTINLT = 169.6 F. MTOUTLT = 139.5 F. MT1 FLOW = 63.7 GPM

\*\*\*\*\* TEMPERATURE (DEGREES F) \*\*\*\*\*  
TEMPCL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGT TEMP 171.50 222.90 166.10 244.80 185.50 239.50 192.80 245.30 181.20 263.70 219.20  
CORRECTED TEMP 167.79 216.31 167.11 237.31 181.63 235.13 192.60 241.71 180.89 261.01 218.12

\*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.416 1.316 1.016 1.720 1.553 1.441

9/ 5/67, TIME = 12.10 TO 12.21 54.8 MW, 17.25 INCHES FROM FULL IN, 510 MICRONS, ROD BNK POS = 21.51 IN.  
FIR TEMP = 135.0 DEG F. MTINLT = 131.2 F. MTOUTLT = 138.0 F. MT1 FLOW = 63.7 GPM

\*\*\*\*\* TEMPERATURE (DEGREES F) \*\*\*\*\*  
TEMPCL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGT TEMP 183.00 171.50 222.90 166.10 244.80 185.50 239.50 192.80 245.30 181.20 263.70 219.20  
CORRECTED TEMP 181.58 216.31 167.11 237.31 181.63 235.13 192.60 241.71 180.89 261.01 218.12

\*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.571 1.416 1.016 1.720 1.553 1.441

9/ 5/67, TIME = 12.27 TO 12.43 54.7 MW, 15.25 INCHES FROM FULL IN, 510 MICRONS, ROD BNK POS = 21.54 IN.  
FIR TEMP = 136.0 DEG F. MTINLT = 131.8 F. MTOUTLT = 138.0 F. MT1 FLOW = 63.7 GPM

\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 TempL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA L88 TEMP 201.80 180.10 243.50 171.90 274.90 200.50 272.90 212.00 286.60 197.50 303.00 237.40  
 CORRECTED TEMP 199.95 177.04 238.01 172.74 265.90 195.06 269.10 211.47 284.59 196.84 248.93 236.68  
 \*\*\*\*\* NUCLEAR HEATING HATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.605 2.461 2.066  
 2.243 1.893 1.761

9/3/67. TIME = 12.50 TO 13.06 54.7 MW, 14.25 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 21.54 IN.  
 P1= TEMP = 136.0 DEG F. MTINTL = 131.1 F. MTOULLT = 140.0 F. MT1 FLOW = 63.7 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 TempL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA L88 TEMP 211.30 183.10 252.90 175.70 290.10 209.00 288.50 219.70 305.90 205.50 324.10 248.80  
 CORRECTED TEMP 208.75 180.30 247.79 176.73 280.46 202.66 284.96 218.90 303.22 204.50 319.00 248.12  
 \*\*\*\*\* NUCLEAR HEATING HATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.808 2.753 2.281  
 2.979 1.893 1.984

9/3/67. TIME = 13.14 TO 13.30 54.0 MW, 13.25 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 21.58 IN.  
 P1= TEMP = 137.0 DEG F. MTINTL = 132.4 F. MTOULLT = 139.0 F. MT1 FLOW = 63.7 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 TempL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA L88 TEMP 218.10 186.20 262.50 180.40 304.90 215.20 300.70 225.70 325.50 214.50 345.30 259.10  
 CORRECTED TEMP 215.27 183.44 257.76 181.50 284.09 208.47 297.01 224.68 322.05 212.99 339.60 258.47  
 \*\*\*\*\* NUCLEAR HEATING HATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.974 3.081 2.262  
 2.804 2.486 2.170

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**corrected** 186.77 208.26 217.26 316.53 235.34 347.68 223.74 362.80 267.81

TEMPERATURE (DEGREES F) = 65.0

WATER FLOW = 63.7 GPM

## NUCLEAR HEATING RATES (MILLIWATTS/GM)

CORRECTED TEMP 236.23 191.01 276.99 185.29 321.97 222.55 329.72 243.20 366.31 231.64 381.86 275.93  
 NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.684 2.281 3.033 2.933 2.493  
 3.439

9/ 9/67. TIME = 15.04 TO 15.20 54.0 MM, 7.75 INCHES FROM FULL IN, 510 MICRONS. RON BNK POS = 21.62 IN.  
 FLN TEMP = 130.0 DEG F. MTINLT = 131.9 F. MTOUTLT = 137.0 F. MT1 FLOW = 63.7 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \*  
 THMCPL NO TEMP 263.70 201.40 306.10 376.10 248.30 371.00 263.30 425.40 260.90 445.90 302.40  
 DATA LBN TEMP  
 CORRECTED TEMP 239.23 198.66 362.00 240.70 366.76 262.21 419.28 257.01 437.11 301.45  
 NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.712 3.213 4.584 3.518  
 4.187

9/ 9/67. TIME = 15.31 TO 15.47 54.0 MM, 4.25 INCHES FROM FULL IN, 750 MICRONS. RON BNK POS = 21.62 IN.  
 FLN TEMP 130.0 DEG F. MTINLT = 132.6 F. MTOUTLT = 136.0 F. MT1 FLOW = 63.6 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \*  
 THMCPL NO TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LBN TEMP 274.10 203.70 317.30 198.60 397.70 260.40 391.30 271.30 450.20 272.30 472.20 314.00  
 CORRECTED TEMP 269.19 200.96 313.37 199.21 303.28 252.39 387.22 270.18 443.24 267.76 462.24 312.58  
 NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.449 2.942 4.537 4.968 3.776  
 3.022

9/ 9/67. TIME = 15.55 TO 16.11 55.0 MM, 2.25 INCHES FROM FULL IN, 750 MICRONS. RON BNK POS = 21.62 IN.

SLR TEMP = 138.0 DEG F. MT1LT = 133.4 F. MT1 FLOW = 63.6 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA L88 TEMP 276.20 206.50 321.50 199.10 402.30 262.80 396.90 276.30 458.90 277.10 478.60 316.50  
CORRECTED TEMP 273.30 203.76 317.18 199.69 387.87 254.70 392.75 275.16 452.44 272.28 468.77 315.00  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* DATA CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* CORRECTED TEMP 274.08 203.36 314.00 198.56 386.27 254.51 392.35 275.85 451.56 271.34 466.42 311.80  
\*\*\*\*\* 2.962 3.663 3.831  
\*\*\*\*\* 5.087 5.620 3.232

9/ 5/67. TIME = 16.15 TO 16.31 54.8 MM. .25 INCHES FROM FULL IN, 750 MICRONS, RON BNK POS = 21.62 IN.

SLR TEMP = 137.0 DEG F. MT1LT = 133.4 F. MT1 FLOW = 63.6 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA L88 TEMP 278.90 206.10 318.90 197.90 400.70 262.60 396.50 277.00 458.00 276.10 476.30 313.20  
CORRECTED TEMP 274.08 203.36 314.00 198.56 386.27 254.51 392.35 275.85 451.56 271.34 466.42 311.80  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* DATA CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* CORRECTED TEMP 274.08 203.36 313.08 197.57 386.97 254.12 391.25 275.26 451.56 271.43 465.91 311.71  
\*\*\*\*\* 2.899 3.663 3.831  
\*\*\*\*\* 5.083 5.620 3.232

9/ 5/67. TIME = 16.38 TO 16.59 55.0 MM. 0.00 INCHES FROM FULL IN, 750 MICRONS, RON BNK POS = 21.62 IN.

SLR TEMP = 138.0 DEG F. MT1LT = 133.9 F. MT1 FLOW = 63.6 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA L88 TEMP 279.10 205.00 317.90 197.20 399.40 262.20 395.40 276.40 458.00 276.20 475.80 313.10  
CORRECTED TEMP 274.29 203.04 313.08 197.57 386.97 254.12 391.25 275.26 451.56 271.43 465.91 311.71  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* DATA CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*

9/8/67. TIME = 0.20 TO 0.3155.3 sec. 39.16 INCHES FROM FULL IN. 750 MICRONS. RON BNK POS = 22.04 IN.  
 P11 126.0 F. M11 127.2 F. M11L = 136.0 F. M11 FLOW = 63.0 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 NEAR 5.06 FAR 3.078 2.913 A  
 NEAR 5.06 FAR 3.078 2.913 A

9/8/67. TIME = 0.33 TO 0.54 55.0 sec. 0.00 INCHES FROM FULL IN. 750 MICRONS. RON BNK POS = 21.99 IN.  
 P11 TEMP = 131.0 DEG F. M11 = 120.3 F. M11L = 133.0 F. M11 FLOW = 63.7 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •  
 DATA TEMP = 131.0 DEG F. M11 = 127.0 F. M11L = 136.0 F. M11 FLOW = 63.8 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •  
 DATA TEMP = 131.0 DEG F. M11 = 127.0 F. M11L = 136.0 F. M11 FLOW = 63.9 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •

MIDDLE CYLINDER MIDDLE CYLINDER MIDDLE CYLINDER  
 NEAR CYLINDER MIDDLE CYLINDER MIDDLE CYLINDER  
 NEAR CYLINDER MIDDLE CYLINDER MIDDLE CYLINDER  
 NEAR CYLINDER MIDDLE CYLINDER MIDDLE CYLINDER

3.125

3.796

5.007

2.886

3.505

4.626

3.096

3.

COLLECTED TEMP = 270.99 201.06 311.45 196.80 302.14 250.07 307.82 271.87 448.28 269.64 464.69 310.00  
 DATA LOG TEMP = 275.99 203.89 315.28 196.60 306.30 258.00 391.90 273.00 455.00 274.30 474.60 311.30  
 DATA LOG TEMP = 131.0 DEG F. M11 = 120.3 F. M11L = 133.0 F. M11 FLOW = 63.7 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •  
 DATA LOG TEMP = 131.0 DEG F. M11 = 127.0 F. M11L = 136.0 F. M11 FLOW = 63.8 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •

3.125

3.796

5.007

2.886

3.505

4.626

3.096

3.

9/8/67. TIME = 0.33 TO 0.54 55.0 sec. 0.00 INCHES FROM FULL IN. 750 MICRONS. RON BNK POS = 21.99 IN.  
 P11 TEMP = 131.0 DEG F. M11 = 120.3 F. M11L = 133.0 F. M11 FLOW = 63.7 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •  
 DATA TEMP = 131.0 DEG F. M11 = 127.0 F. M11L = 136.0 F. M11 FLOW = 63.8 GPM  
 • • • • • TEMPERATURE (DEGREES F) • • • • •

3.125

3.796

5.007

2.886

3.505

4.626

3.096

3.

三

9/ 0/67, TIME = 9.09 10 9.19 55.4 MW. 19.16 INCHFS FROM FULL IN. 750 MICRONS, ROD BNK POS = 22.07 IN.

MT1 TEMP = 132.0 DEG F, MT1INL1 = 138.0 F. MT1FLW = 63.7 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 170.60 166.16 202.40 157.40 216.46 172.40 215.10 179.70 213.30 166.60 226.80 199.60  
CORRECTED TEMP 168.81 160.29 196.36 158.68 210.00 169.08 211.84 180.01 208.95 166.17 224.83 198.31  
NUCLEAR HEATING HATES (WATTS/GMH) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.009 1.071 1.077 1.077 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071  
1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096 1.096

9/ 0/67, TIME = 9.24 10 9.35 56.4 MW. 17.16 INCHFS FROM FULL IN. 510 MICRONS, ROD BNK POS = 22.10 IN.

MT1 TEMP = 138.0 DEG F, MT1INL1 = 130.8 F. MT1FLW = 63.6 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 167.00 172.70 224.70 165.60 246.50 187.50 245.10 197.00 249.80 182.70 267.90 220.40  
CORRECTED TEMP 165.00 169.32 210.16 166.63 238.93 183.24 240.82 196.70 246.27 182.56 265.09 219.33  
NUCLEAR HEATING HATES (WATTS/GMH) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071  
1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071 1.071

9/ 0/67, TIME = 9.42 10 9.57 56.4 MW. 15.16 INCHFS FROM FULL IN. 510 MICRONS, ROD BNK POS = 22.13 IN.

MT1 TEMP = 138.0 DEG F, MT1INL1 = 130.6 F. MT1FLW = 63.6 GPM

TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 202.90 179.10 266.60 173.30 277.70 202.70 274.80 212.60 287.60 197.40 307.60 241.00  
CORRECTED TEMP 200.71 176.03 239.61 174.01 268.65 197.03 271.03 212.05 285.58 196.44 303.30 240.29

\*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.491 1.492 1.493  
2.071 2.075 2.079

9/ 6/67. TIME = 10.06 TO 10.22 54.1 MW. 14.16 INCHFS FROM FULL IN. 550 MICRONS. ROD BNK POS = 22.015 IN.  
FIX TEMP = 135.0 REG F. MTINLT = 131.1 F. MTOUTLT = 139.0 F. MT1 FLOW = 63.6 GPM  
\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 212.10 183.90 255.70 177.40 292.00 209.00 249.20 222.00 310.70 208.30 327.90 249.70  
CORRECTED TEMP 209.52 181.11 250.70 178.3H 282.27 202.66 285.68 221.12 307.83 207.14 322.61 249.03  
\*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
2.095 2.113 1.800  
2.0835 2.0974 2.0717

9/ 6/67. TIME = 10.29 TO 10.45 54.1 MW. 13.16 INCHFS FROM FULL IN. 550 MICRONS. ROD BNK POS = 22.119 IN.  
FIX TEMP = 136.0 REG F. MTINLT = 131.9 F. MTOUTLT = 137.0 F. MT1 FLOW = 63.6 GPM  
\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 219.30 186.40 263.30 180.30 305.40 215.40 302.30 228.90 328.30 216.30 347.00 258.30  
CORRECTED TEMP 216.42 183.64 258.60 181.40 294.56 208.67 298.60 228.04 324.72 214.69 341.23 257.66  
\*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
2.0836 2.0952 2.0716  
2.0533 3.0146 2.0715

9/ 6/67. TIME = 10.51 TO 11.07 54.1 MW. 12.6H INCHES FROM FULL IN. 550 MICRONS. ROD BNK POS = 22.22 IN.

FIX TEMP = 136.0 DEG F. HTINLT = 131.5 F. HTOUTLT = 137.0 F. HT1 FLOW = 53.6 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 \*  
 DATA LGR TEMP 225.00 188.30 267.70 181.30 314.00 219.50 310.90 233.40 339.60 219.90 10 11 12  
 CORRECTED TEMP 221.88 185.35 263.17 182.37 302.48 212.62 307.07 232.45 336.03 218.08 351.37 262.68  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.015 2.048 2.394 3.344 2.055 2.271

9/ 6/67. TIME = 11.12 TO 11.28 54.2 MW, 12.16 INCHES FROM FULL IN, 550 MICRONS, ROD BNK POS = 22.22 IN.  
 FIX TEMP = 136.0 DEG F. HTINLT = 131.8 F. HTOUTLT = 136.0 F. HT1 FLOW = 63.6 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 \*  
 DATA LGR TEMP 230.90 190.00 273.70 183.70 323.80 224.60 320.30 238.50 352.40 226.00 10 11 12  
 CORRECTED TEMP 227.80 187.07 269.41 184.91 311.53 217.55 316.33 237.53 348.35 223.83 364.81 269.21  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.184 2.504 2.162 3.524 2.772 2.393

9/ 6/67. TIME = 11.34 TO 11.50 54.1 MW, 11.16 INCHES FROM FULL IN, 510 MICRONS, ROD BNK POS = 22.25 IN.  
 FIX TEMP = 136.0 DEG F. HTINLT = 131.5 F. HTOUTLT = 136.0 F. HT1 FLOW = 63.6 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 \*  
 DATA LGR TEMP 238.70 193.70 280.90 186.20 335.00 229.30 331.50 245.00 370.50 234.00 388.30 276.50  
 CORRECTED TEMP 235.20 190.80 276.89 187.33 321.85 222.36 327.38 244.00 365.73 231.64 380.90 275.93  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.048 2.394 2.162 3.344 2.055 2.271

3.436

2.059

3.437

2.057

2.947

2.506

9/ 6/67. TIME = 11.58 TO 12.19 54.2 MW. 7.68 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.25 IN.  
FIX TEMP = 137.0 DEG F. HTINLT = 131.9 F. HTOUTL = 136.0 F. HT1 FLOW = 63.6 GPM

THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 264.30 201.30 304.80 194.90 375.00 249.10 370.30 264.40 424.20 260.30 444.10 301.50  
CORRECTED TEMP 259.80 198.56 301.22 195.36 360.91 241.48 366.06 263.31 418.10 256.44 435.36 300.58  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
4.156 2.692 3.170  
4.061 3.509 2.980

9/ 6/67. TIME = 12.20 TO 12.36 54.1 MW. 4.16 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.25 IN.  
FIX TEMP = 137.0 DEG F. HTINLT = 133.5 F. HTOUTL = 136.0 F. HT1 FLOW = 63.6 GPM

THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 275.40 200.10 315.60 197.10 391.90 256.90 388.70 274.40 448.80 272.30 466.80 310.90  
CORRECTED TEMP 270.48 202.36 311.81 197.47 377.85 249.01 384.63 273.26 441.87 267.76 456.81 309.61  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
4.475 3.433 2.869  
4.946 3.786 3.164

9/ 6/67. TIME = 12.44 TO 13.00 54.2 MW. 2.16 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.25 IN.  
FIX TEMP = 138.0 DEG F. HTINLT = 132.8 F. HTOUTL = 133.5 F. HT1 FLOW = 63.5 GPM

THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
\*\*\*\*\* TEMPERATURE (DEGREES F) \*\*\*\*\*

DATA LGR TEMP 276.30 203.40 314.90 196.10 395.10 260.30 391.70 276.10 451.50 272.00 468.90 311.80  
 CORRECTED TEMP 271.41 200.66 311.17 196.50 380.96 252.29 387.62 274.96 444.52 267.47 458.88 310.49  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 4.545 3.427 2.926 3.021  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 5.031 3.793 3.239

9/ 6/87. TIME = 13.09 TO 13.25 54.2 MW. .16 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.27 IN.  
 FIX TEMP = 138.0 CES F. MTINLT = 132.5 F. MTOUTLT = 136.0 F. MTI FLOW = 63.1 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 275.50 202.10 313.50 195.50 393.70 259.70 389.90 274.50 450.10 271.70 467.70 309.40  
 CORRECTED TEMP 270.58 199.36 309.89 195.92 379.58 251.71 385.83 273.36 443.15 267.19 457.69 308.16  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 4.524 3.001 2.890 5.008  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 5.008 3.764 3.199

9/ 6/87. TIME = 13.31 TO 13.52 54.3 MW. 0.00 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.27 IN.  
 FIX TEMP = 137.0 CES F. MTINLT = 132.2 F. MTOUTLT = 136.0 F. MTI FLOW = 63.5 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 275.50 202.30 313.20 195.60 394.30 259.39 390.90 274.70 450.90 272.20 468.10 309.30  
 CORRECTED TEMP 270.58 199.56 309.62 196.02 380.17 251.32 386.82 273.56 443.93 267.66 458.08 307.77  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 4.542 3.436 2.857 5.016  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 5.016 3.794 3.157

9/7/67. TIME = 9.59 TO 9.11 55.1 MM. 44.12 INCHFS FWUM FULL IN. 520 MICRONS. ROD BNK POS = 22.79 IN.  
F1X TEMP = 129.0 DEG F. MTINLT = 127.3 F. MTOUTLT = 137.0 F. MT1 FLOW = 63.8 GPM

F1X TEMP NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 137.00 140.10 135.60 134.50 136.10 134.30 135.40 136.30 135.00 134.50 135.30 135.90  
CORRECTED TEMP 136.30 137.22 128.32 136.48 128.92 126.42 136.88 135.14 133.59 134.94 135.30 132.38  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER FAR CYLINDER \*\*\*\*\*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 136.70 141.80 137.70 135.10 137.10 135.20 137.40 136.50 137.00 135.40 137.30 136.70  
CORRECTED TEMP 137.93 138.85 130.64 137.06 130.04 127.44 130.76 137.28 135.62 135.81 137.25 133.20  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER FAR CYLINDER \*\*\*\*\*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 141.60 143.30 147.20 139.70 150.80 142.10 149.80 142.10 141.60 137.30 146.00 148.10  
CORRECTED TEMP 140.72 140.28 141.16 141.52 145.39 135.26 150.36 142.76 143.37 137.66 147.66 144.89

9/7/67. TIME = 9.14 TO 9.25 59.0 MM. 39.12 INCHES FROM FULL IN. 520 MICRONS. ROD BNK POS = 22.81 IN.  
F1X TEMP = 131.0 DEG F. MTINLT = 127.2 F. MTOUTLT = 138.0 F. MT1 FLOW = 63.7 GPM  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 138.70 141.80 137.70 135.10 137.10 135.20 137.40 136.50 137.00 135.40 137.30 136.70  
CORRECTED TEMP 137.93 138.85 130.64 137.06 130.04 127.44 130.76 137.28 135.62 135.81 137.25 133.20  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER NEAR CYLINDER FAR CYLINDER \*\*\*\*\*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 141.60 143.30 147.20 139.70 150.80 142.10 149.80 142.10 141.60 137.30 146.00 148.10  
CORRECTED TEMP 140.72 140.28 141.16 141.52 145.39 135.26 150.36 142.76 143.37 137.66 147.66 144.89

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
•110 •115 •120 •124

9/ 7/67. TIME = 10.02 TO 10.13 54.0 MW, 24.12 INCHES FROM FULL IN.  
RIN TEMP = 132.0 DEG F. MTINL = 168.3 F. MTOUTL = 139.0 F. MTI FLOW = 63.6 GPM

• • • • • • • TEMPERATURE (DEGREES F) • • • • • • •  
TMCP1 NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 148.40 150.00 165.60 145.40 170.50 151.00 168.10 152.90 163.30 146.20 170.80 165.20  
CORRECTED TEMP 147.26 147.25 161.53 147.05 167.36 145.35 167.49 153.31 160.25 146.32 169.84 162.43  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
•349 •373 •383 •628 •634

9/ 7/67. TIME = 10.24 TO 10.35 54.0 MW, 19.12 INCHES FROM FULL IN.  
RIN TEMP = 132.0 DEG F. MTINL = 169.9 F. MTOUTL = 140.0 F. MTI FLOW = 63.6 GPM  
• • • • • • • TEMPERATURE (DEGREES F) • • • • • • •  
TMCP1 NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 171.10 165.60 206.00 160.40 219.90 174.10 217.30 180.30 217.50 169.60 231.90 201.40  
CORRECTED TEMP 169.30 161.81 199.58 161.59 213.33 170.91 213.88 180.60 213.22 169.09 230.07 200.13  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
•110 •109 •998 1.252 1.214 1.093

9/ 7/67. TIME = 10.43 TO 10.54 54.0 MW, 17.12 INCHES FROM FULL IN.  
RIN TEMP = 134.0 DEG F. MTINL = 168.9 F. MTOUTL = 139.0 F. MTI FLOW = 63.6 GPM

\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 105.30 171.30 223.40 165.90 246.30 186.30 244.00 195.00 248.20 181.60 265.10 219.00  
 CORRECTED TEMP 103.81 167.58 216.03 166.92 238.74 182.35 239.70 195.53 244.65 181.48 262.37 217.92  
 \*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 1.611 1.478 1.316 1.621 1.767 1.444

9/7/67. TIME = 11.02 TO 11.18 54.5 MW, 15.12 INCHES FROM FULL IN, 510 MICRONS. RDN BNK POS = 22.92 IN.  
 FIX TEMP = 135.0 DEG F. MTINLT = 149.0 F. MTOUTLT = 139.0 F. MT1 FLOW = 63.6 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 203.70 180.10 244.50 172.50 276.80 201.70 275.40 214.60 290.10 198.70 305.60 238.70  
 CORRECTED TEMP 201.47 177.04 239.05 173.63 267.79 196.13 271.64 213.98 288.06 197.99 301.43 237.98  
 \*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 2.295 1.912 1.628 ? .526 2.105 1.792

9/7/67. TIME = 11.26 TO 11.42 54.9 MW, 14.12 INCHES FROM FULL IN, 520 MICRONS. RDN BNK POS = 22.99 IN.  
 FIX TEMP = 134.0 REG F. MTINLT = 130.8 F. MTOUTLT = 137.0 F. MT1 FLOW = 63.5 GPM  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 212.30 183.40 256.70 176.30 295.40 210.10 290.50 221.70 312.70 209.10 330.70 251.40  
 CORRECTED TEMP 209.71 180.61 251.74 179.46 285.51 203.64 287.00 220.83 309.72 207.90 325.29 250.73  
 \*\*\*\*\* NUCLEAR HEATING WATTS (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 2.622 2.146 1.637 ? .892 2.026

9/ 7/67. TIME = 11.51 TO 12.07 54.5 MM. 13.12 INCHES FROM FULL IN. 520 MICRONS. ROD BNK POS = 22.99 IN.

FIX TEMP = 136.0 DEG F. MTINLT = 130.4 F. MTOURLT = 137.0 F. MT1 FLOW = 63.6 GPM  
THMCPL NO 1 2 3 4 5 6 7 \*  
DATA LGR TEMP 223.10 188.10 266.60 181.50 311.60 217.70 307.80 232.20 336.10 218.70 352.70 261.50  
CORRECTED TEMP 220.06 185.15 262.03 182.56 300.29 210.89 303.99 231.25 332.24 216.95 346.62 260.87  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
2.955 2.371 2.001 3.253 2.610 2.203

9/ 7/67. TIME = 12.21 TO 12.37 54.4 MM. 12.62 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 22.99 IN.

FIX TEMP = 137.0 DEG F. MTINLT = 130.5 F. MTOURLT = 138.0 F. MT1 FLOW = 63.5 GPM  
THMCPL NO 1 2 3 4 5 6 7 \*  
DATA LGR TEMP 227.50 190.50 273.20 181.90 317.50 220.80 314.10 236.00 346.00 223.00 361.10 264.90  
CORRECTED TEMP 224.50 187.50 265.77 182.95 305.70 213.88 310.21 235.04 342.19 221.00 354.63 264.29  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
3.1n2 2.466 2.053 3.422 2.696 2.264

9/ 7/67. TIME = 12.51 TO 13.07 54.5 MM. 12.12 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 23.01 IN.

FIX TEMP = 136.0 DEG F. MTINLT = 131.5 F. MTOURLT = 137.0 F. MT1 FLOW = 63.5 GPM  
THMCPL NO 1 2 3 4 5 6 7 \*  
DATA LGR TEMP 231.70 191.50 275.60 183.90 325.50 224.70 322.30 240.20 356.40 228.10 372.00 269.90

CORRECTED TEMP 22H.57 1MH.59 271.32 185.11 313.11 217.65 318.32 239.22 352.19 226.08 365.00 269.31  
 FIX TEMP = 136.0 REG F. MTLNLT = 140.5 F. HTUULT = 137.0 F. HT1 FLOW = 63.5 GPM  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 241.50 145.20 203.50 105.00 334.10 231.40 336.20 247.90 375.10 235.50 390.30 278.70  
 CORRECTED TEMP 237.96 192.12 279.55 106.94 326.00 224.39 332.01 246.88 370.15 233.06 382.82 278.14  
 FIX TEMP = 130.0 REG F. MTLNLT = 132.3 F. HTUULT = 135.0 F. HT1 FLOW = 63.5 GPM  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 266.00 203.00 307.80 195.70 378.70 250.20 373.90 267.30 428.60 263.10 446.90 302.40  
 CORRECTED TEMP 261.43 200.29 304.23 196.12 304.95 242.54 369.60 266.20 422.42 259.08 438.08 301.45  
 FIX TEMP = 130.0 REG F. MTLNLT = 130.5 F. HTUULT = 140.0 F. HT1 FLOW = 63.5 GPM  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 3.213 2.683 3.214 2.542 3.206 2.548 3.571 2.005 2.359 2.051 2.993 3.051 2.534  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER

9/7/67. TIME = 14.13 TO 14.29 54.6 min. 4.12 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.03 IN.

FLX TEMP = 139.0 DEG F. HTINLT = 132.8 F. HTOUTLT = 137.0 F. HT1 FLOW = 63.6 GPM

\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*

TMPCPL NO 1	2	3	4	5	6	7	8	9	10	11	12
DATA LSR TEMP 275.80	205.10	317.90	199.60	396.70	260.50	391.60	276.20	450.80	273.80	470.70	314.40
CORRECTED TEMP 270.89	202.36	313.88	200.17	382.53	252.48	387.52	275.06	443.83	269.17	460.71	312.97

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*

\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER

4.512 3.011 2.921 4.958 3.781 3.210

9/7/67. TIME = 14.48 TO 14.58 54.9 min. 2.12 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.06 IN.

FLX TEMP = 139.0 DEG F. HTINLT = 130.0 F. HTOUTLT = 137.0 F. HT1 FLOW = 63.5 GPM

\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*

TMPCPL NO 1	2	3	4	5	6	7	8	9	10	11	12
DATA LSR TEMP 278.20	206.00	318.70	199.00	399.10	262.40	393.40	277.70	454.20	274.70	473.30	314.10
CORRECTED TEMP 273.36	203.26	314.61	199.59	384.67	254.32	389.26	276.55	447.50	270.02	463.36	312.68

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*

\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER

3.446 2.890 5.038 3.801 3.188 3.081

9/7/67. TIME = 15.11 TO 15.32 54.3 min. 0.00 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.07 IN.

FLX TEMP = 140.0 DEG F. HTINLT = 133.4 F. HTOUTLT = 138.0 F. HT1 FLOW = 63.6 GPM

\* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*

TMPCPL NO 1	2	3	4	5	6	7	8	9	10	11	12
DATA LSR TEMP 277.80	203.90	314.50	196.60	396.30	261.60	392.70	276.80	453.10	273.80	470.80	311.70
CORRECTED TEMP 272.95	201.16	310.81	196.99	382.14	253.55	388.57	275.65	446.42	269.17	460.81	310.39

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*

9/ 8/67. TIME = 9.22 10 9.31 54.9 MW. 44.80 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 23.50 IN.  
FLX TEMP = 131.0 DEG F. MTINLT = 128.5 F. MTOUTL = 128.0 F. MT1 FLOW = 63.8 GPM  
CORRECTED TEMP 136.98 137.09 129.98 138.23 130.26 128.80 137.02 136.11 134.00 136.50 137.05 134.02  
NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER  
-0.061 0.136 -0.105 -0.066 -0.149 -0.114

\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER  
4.552 3.622 2.911  
5.030 3.781  
3.216

\*\*\*\*\* NORMALIZED TO 40 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER  
5.030 3.781

9/ 8/67. TIME = 9.41 7:0 9.50 54.7 MW. 39.80 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 23.60 IN.  
FLX TEMP = 133.0 DEG F. MTINLT = 128.1 F. MTOUTL = 138.0 F. MT1 FLOW = 63.8 GPM  
CORRECTED TEMP 137.70 140.80 137.10 136.30 137.30 135.40 136.40 137.02 136.70 139.60 138.40 137.60 135.00 136.30 136.70  
TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 140.70 142.50 137.20 134.60 137.10 136.70 139.60 138.40 137.60 139.00 138.40 137.60 135.00 136.30 136.70  
CORRECTED TEMP 139.85 139.52 130.06 136.58 130.06 129.14 140.01 139.14 136.24 135.43 136.28 133.20  
NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAIR CYLINDER  
-0.036 .163 .126 -.040 .179 -.138

9/ 8/67. TIME = 10.02 TO 10.11 54.7 MW. 29.80 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 23.63 IN.  
FLX TEMP = 133.0 DEG F. MTINLT = 129.1 F. MTOUTL = 139.0 F. MT1 FLOW = 63.8 GPM

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MH \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* .037 .108 .209 .099 \*\*\*\*\*  
 THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 142.30 145.40 147.60 139.80 148.30 141.20 147.40 142.30 145.90 140.10 147.30 146.50  
 CORRECTED TEMP 141.39 142.29 141.60 141.62 142.59 134.24 148.11 142.95 144.69 140.39 146.98 143.25

9/ 8/67, TIME = 10.39 TO 10.48 54.4 MM. 19.80 INCHES FROM FULL IN. 510 MICRONS. RUN BNK POS = 23.67 IN.  
 FIX TEMP = 133.0 DEG F. HTINLT = 130.4 F. HTOUTLT = 138.0 F. HT1 FLOW = 65 GPM  
 THMCPL NO DATA LGR TEMP CORRECTED TEMP  
 167.30 163.50 198.80 159.46 193.15 159.61  
 169.60 210.00 203.00 203.93 203.93 205.29  
 204.70 164.10 163.74 200.41 163.74 215.98 194.1  
 \*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*  
 \*\*\*\* AT INDICATED POWER \*\*\*\*  
 \*\*\*\* NORMALIZED TO 60 MW \*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 NEAR CYLINDER FAR CYLINDER  
 1.024 1.094 1.024 1.094  
 0.91 0.928 0.91 0.928

9/ 8/67. TIME = 10.56 TO 11.05 54.4 MW, 17.80 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 23.70 IN.  
FIX TEMP = 134.0 DEG F. HTINLT = 131.0 F. HTOUTLT = 139.0 F. HT1 FLOW = 63.8 GPM

THWCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	180.90	171.90	217.10	164.10	234.40	180.30	232.20	190.70	235.40	178.20	250.20	211.10
CORECTED TEMP	179.33	168.19	210.28	165.18	227.41	176.72	227.90	190.76	232.17	177.97	247.87	209.95
***** NUCLEAR HEATING RATES (WATTS/GM) ***** ***** AT INDICATED POWER ***** ***** NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER ***** 1.390 1.323 1.124 1.534 1.459 1.240												

9/ 8/67. TIME = 11.12 TO 11.21 54.4 MW, 15.90 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 23.71 IN.  
FIX TEMP = 135.0 DEG F. HTINLT = 131.1 F. HTOUTLT = 138.0 F. HT1 FLOW = 63.8 GPM

THWCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	196.90	178.40	236.70	171.30	265.00	195.80	262.20	206.80	271.90	193.00	289.60	231.60
CORECTED TEMP	194.65	175.32	230.95	172.16	256.56	190.56	258.22	206.46	268.70	192.16	286.23	230.86
***** NUCLEAR HEATING RATES (WATTS/GM) ***** ***** AT INDICATED POWER ***** ***** NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER ***** 1.956 1.736 1.484 2.157 1.915 1.637												

9/ 8/67. TIME = 11.28 TO 11.37 54.3 MW, 14.90 INCHES FROM FULL IN. 510 MICRONS. ROD BNK POS = 23.73 IN.  
FIX TEMP = 135.0 DEG F. HTINLT = 131.9 F. HTOUTLT = 139.0 F. HT1 FLOW = 63.7 GPM

THWCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	203.80	180.90	248.00	176.00	281.10	203.40	276.80	214.30	293.80	202.30	312.60	243.60

CORRECTED TEMP 201.57 177.85 242.64 177.02 271.89 197.65 273.06 213.69 291.73 201.45 308.06 242.90  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 1.944 1.701 2.590 2.148  
 2.344

9/ 8/67, TIME = 11.45 TO 11.54 54.4 MW. 13.80 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.73 IN.  
 FIX TEMP = 136.0 DEG F. HTINLT = 130.9 F. HTOUTLT = 138.0 F. HT1 FLOW = 63.7 GPM  
 \*\*\*\*\* \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THWCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 215.40 184.50 259.80 160.00 300.40 213.30 295.20 226.10 318.00 212.10 336.40 254.60  
 CORRECTED TEMP 212.68 181.72 254.96 181.11 289.94 206.64 291.78 225.07 314.82 210.73 330.72 253.95  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.198 1.884 2.955 2.413  
 2.679 2.005 2.527 2.078

9/ 8/67, TIME = 12.02 TO 12.11 54.3 MW. 13.40 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.76 IN.  
 FIX TEMP = 137.0 DEG F. HTINLT = 131.9 F. HTOUTLT = 139.0 F. HT1 FLOW = 63.7 GPM  
 \*\*\*\*\* \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 THWCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 220.00 185.60 263.40 161.10 309.60 218.40 304.50 230.20 328.80 216.20 346.30 260.30  
 CORRECTED TEMP 217.09 182.83 258.70 182.17 298.43 211.56 300.75 229.29 325.21 214.59 340.56 259.67  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.841 2.287 3.040 2.527 2.005 2.527 2.215

9/ 8/67, TIME = 12.17 TO 12.26 54.3 MW. 12.80 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 23.76 IN.

FIX TEMP = 137.0 DEG F. HTINLT = 131.2 F. HTOUTLT = 138.0 F. HTI FLOW = 63.7 GPM

THMCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	226.50	189.20	268.80	182.00	315.90	222.00	312.60	235.70	340.90	220.30	357.00	263.80
CORRECTED TEMP	223.32	186.20	264.31	183.05	304.25	215.04	308.71	234.74	337.29	218.46	350.74	263.18
NEAR CYLINDER	3.024	2.376	2.040	3.342	2.552	2.181	3.040	2.625	3.642	2.820	3.410	2.954

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* 2.254

9/ 8/67. TIME = 12.31 TO 12.40 54.3 MM. 11.80 INCHES FROM FULL IN. 510 MICRONS. HTN BNK POS = 23.78 IN.

FIX TEMP = 134.0 DEG F. HTINLT = 131.2 F. HTOUTLT = 139.0 F. HTI FLOW = 63.7 GPM

THMCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	234.80	192.90	277.60	185.20	330.20	228.70	326.60	243.80	360.90	229.90	377.70	272.60
CORRECTED TEMP	231.54	189.79	273.46	186.36	317.45	221.78	322.55	242.80	356.51	227.78	370.82	272.02
NEAR CYLINDER	3.296	2.552	2.181	3.642	2.820	3.410	2.954	3.040	2.625	3.040	2.820	3.410

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
\*\*\*\*\* 2.410

9/ 8/67. TIME = 13.08 TO 13.17 54.5 MM. 8.040 INCHES FROM FULL IN. 510 MICRONS. HTN BNK POS = 23.79 IN.

FIX TEMP = 137.0 DEG F. HTINLT = 132.2 F. HTOUTLT = 137.0 F. HTI FLOW = 63.7 GPM

THMCPL NO	1	2	3	4	5	6	7	8	9	10	11	12
DATA LGR TEMP	261.30	200.30	301.90	194.20	371.20	248.30	366.40	263.50	416.60	256.00	434.70	297.80
CORRECTED TEMP	256.43	197.56	294.32	194.66	357.22	240.70	362.23	262.41	410.64	252.39	425.62	296.99
NEAR CYLINDER	3.024	2.376	2.040	3.342	2.552	2.181	3.040	2.625	3.642	2.820	3.410	2.954

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* 2.410

C-31

TEMPERATURE, °C	100	200	300	400	500	600	700	800	900	1000	1100	1200
COEFFICIENT OF EXPANSION, °C⁻¹	2.20-02	2.20-00	3.11-02	4.67-02	3.42-01	2.53-01	3.08-02	2.76-02	4.45-01	2.67-02	4.59-02	3.10-02
MIDDLE CYLINDER	2.00-02	2.00-00	3.11-02	4.67-02	3.42-01	2.53-01	3.08-02	2.76-02	4.45-01	2.67-02	4.59-02	3.10-02
FAR CYLINDER	2.00-02	2.00-00	3.11-02	4.67-02	3.42-01	2.53-01	3.08-02	2.76-02	4.45-01	2.67-02	4.59-02	3.10-02
MEAN CYLINDER	2.00-02	2.00-00	3.11-02	4.67-02	3.42-01	2.53-01	3.08-02	2.76-02	4.45-01	2.67-02	4.59-02	3.10-02

9/ 26/67. TIME = 10:15 TO 14:30 500.2 MM. 0.00 INCHES FROM FULL IN. SIP MICRONS, NON BNK POS = 23.03 IN.  
 11/ TEMP = 130.0 deg F. MTRLT = 130.7 F. MTRLT = 137.0 F. MTRLT FLOW = 63.7 GPM  
 CORRECTED TEMP = 203.00 311.91 198.25 379.78 251.52 306.52 275.26 445.31 270.59 459.69 308.74  
 CYLINDER 1 deg C 1 2 3 4 5 6 7 8 9 10 11 12  
 CYLINDER 1 deg F 205.00 315.76 197.61 303.91 259.50 308.60 276.40 452.30 275.30 464.70 310.00  
 CORRECTED 3.017 2.826 0.905 3.776 3.123  
 NUCLEAR HEATING WATES (MARTS/GM) \*\*\*\*\*  
 INDICATED POWER \*\*\*\*\*  
 NUCLEAR CYLINDER \*\*\*\*\*  
 MIDDLE CYLINDER \*\*\*\*\*  
 FAR CYLINDER \*\*\*\*\*  
 NORMALIZED TO 60 MH \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.017 2.826 0.905 3.776 3.123

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CCBRCED TEE 149.21 150.89 151.76 157.53 165.66 165.69 166.54 167.58 169.35 161.50

TEMPERATURE (DEGREES F.)

510 MICRONS. ROT RNK POS = 26.43 IN.

• 0.972	• 0.972	• 0.972	• 0.972
• 0.972	• 0.972	• 0.972	• 0.972
• 0.972	• 0.972	• 0.972	• 0.972
• 0.972	• 0.972	• 0.972	• 0.972

INDICATE HOW MUCH CLARIFYING WATES (INETS/gm) NORMALIZED TO 60 gm

CEDECCTD07E00 101.00 102.10 103.00 104.00 105.00 106.00 107.00 108.00 109.00 110.00 111.00 112.00 113.00 114.00 115.00 116.00 117.00 118.00 119.00 120.00 121.00 122.00 123.00 124.00 125.00 126.00 127.00 128.00 129.00 130.00 131.00 132.00 133.00 134.00 135.00 136.00 137.00 138.00 139.00 140.00 141.00 142.00 143.00 144.00 145.00 146.00 147.00 148.00 149.00 150.00 151.00 152.00 153.00 154.00 155.00 156.00 157.00 158.00 159.00 160.00 161.00 162.00 163.00 164.00 165.00 166.00 167.00 168.00 169.00 170.00 171.00 172.00 173.00 174.00 175.00 176.00 177.00 178.00 179.00 180.00 181.00 182.00 183.00 184.00 185.00 186.00 187.00 188.00 189.00 190.00 191.00 192.00 193.00 194.00 195.00 196.00 197.00 198.00 199.00 200.00

DATA 680 TEMP  
FRONTLNG 142.90 145.20 147.10 150.11 153.11 156.40 163.50 166.50 170.00 173.10 177.10 181.10 185.10 187.50

תְּבִיבָה וְעַמְּלֵה בְּבִירָה וְבְּבִירָה וְעַמְּלֵה וְתְּבִיבָה

011147. TIME = 9.53 TO 10.02 00.0 sec. 29.90 INCHES FROM FUEL IN, 510 MICRONS. RDN BNK POS = 26040 IN.

-027	0000	0000	0000	0000
-027	0000	0000	0000	0000
-027	0000	0000	0000	0000
-027	0000	0000	0000	0000

**CONNECTED TIME** 120.13 **138.56** 131.04 **130.03** 131.37 **129.36** **140.07** **137.07** **136.24** **136.40** **136.22** **136.04**

A TREATISE ON THE HISTORY OF THE CHURCH 3

9/11/07. Time = 5.35 TC 994 6.01 40.00 100% from small In. S10 -ICR005. WDN HHR PUS = 26.38 IN.

9/11/67, TIME = 11.03 TO 11.12 50.6 sec. 16.11 inches from full in. 510 microns, non rank PUS = 26.52 in.

9/11/67, TIME = 10.39 TO 10.39 60.0 sec. 20.10 inches from full in. 510 microns, non rank POS = 26.45 in.

MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.45 in. 1.356

MEAN CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.252 in. 1.358

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.035 in. 1.354

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.355

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.356

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.357

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.358

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.359

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.360

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.361

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.362

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.363

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.364

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.365

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.366

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.367

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.368

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.369

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.370

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.371

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.372

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.373

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.374

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.375

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.376

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.377

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.378

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.379

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.380

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.381

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.382

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.383

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.384

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.385

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.386

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.387

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.388

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.389

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.390

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.391

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.392

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.393

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.394

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.395

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.396

NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER 1.030 in. 1.397

9/11/87, TIME = 11.19 TO 11.28 59.9 SEC. 15.20 INCHES FROM FULL IN.  
 510 MICRONS. NON BNK POS = 26.52 IN.  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 5 6 7 8 9 10 11 12  
 THERM 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LOG TEMP 199.16 180.80 243.50 173.20 272.90 199.70 268.90 210.30 279.90 196.40 297.70 238.40  
 CORRECTED TEMP 197.07 176.94 238.01 174.31 264.08 194.35 265.03 209.83 277.34 195.47 293.89 237.68  
 \*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* 1.612 1.824 2.110 1.827 1.615

9/11/87, TIME = 11.19 TO 11.28 59.9 SEC. 14.20 INCHES FROM FULL IN.  
 510 MICRONS. NON BNK POS = 26.57 IN.  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 5 6 7 8 9 10 11 12  
 THERM 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LOG TEMP 203.50 183.50 252.90 177.00 287.00 207.30 283.90 218.90 301.10 203.80 316.20 247.50  
 CORRECTED TEMP 205.59 180.71 247.79 177.99 278.27 201.14 280.29 218.13 298.61 202.89 311.51 246.82  
 \*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 \*\*\*\*\* 2.030 2.032 2.033 2.034 2.035 2.036 2.037 2.038 2.039 2.040 2.041 2.042

9/11/87, TIME = 11.35 TO 11.44 59.5 SEC. 14.20 INCHES FROM FULL IN.  
 510 MICRONS. NON BNK POS = 26.57 IN.  
 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \*  
 5 6 7 8 9 10 11 12  
 THERM 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LOG TEMP 218.70 187.80 264.30 186.50 306.40 216.30 303.70 230.80 325.30 213.90 341.40 260.00  
 CORRECTED TEMP 215.80 184.80 259.64 181.54 295.40 209.54 299.95 229.87 321.86 212.42 335.90 259.37  
 \*\*\*\*\* NUCLEAR HEATING WATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER \*\*\*\*\*  
 \*\*\*\*\* 1.824 2.110 1.827 1.615 1.824 2.110 1.827 1.615 1.824 2.110 1.827 1.615

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510 MICRONS. RON BNK PUS = 26.59 IN.

3.162 2.487 2.187 3.147 2.491 2.191  
MAUL CVLAMINEN VÄÄN LYLINDEX

WATTS INPUTTED TO THE CIRCUIT BY THE POWER SUPPLY

**CORRECTED ITEM** 223.02 105.39 271.09 106.46 313.58 219.94 317.82 239.32 344.28 221.05 359.67 271.

DATA LGR TEMP 228.00 191.30 275.90 185.39 329.00 227.10 321.00 222.30 315.70 211.00 300.00 200.00 290.00 190.00 280.00 180.00 270.00 170.00 260.00 160.00 250.00 150.00 240.00 140.00 230.00 130.00 220.00 120.00 210.00 110.00 200.00 100.00 190.00 90.00 180.00 80.00 170.00 70.00 160.00 60.00 150.00 50.00 140.00 40.00 130.00 30.00 120.00 20.00 110.00 10.00 100.00 0.00

$$\text{Flow} = 134.0 \text{ ft. } \times 11 \text{ gpm} = 63.6 \text{ GPM}$$

11/16. TYPE = 12.07 T0 12.16 59.6 MV. 13.20 INCHES FROM FULL IN. 510 MICRONS. ROT BNK POS = 24.57 IN

	FRONT CYLINDER	MIDDLE CYLINDER	Rear CYLINDER
MEAN CYLINDER	2.053	3.048	2.053
STANDARD CYLINDER	2.077	3.048	2.053
MAX CYLINDER	2.068	3.049	2.053

**NUCLEAR REACTING RATES (ATTS/SEC) INDICATED FOR THE INDIVIDUAL ELEMENTS**

COMPUTER SYSTEMS

DATA LINE ITEM

01/11/67. T116 = 11.51 TO 12.00 00.0. 13.00 Imports from India. 510 MICROS. MON HNK PUS = 26.56 IN.

2.003 2.295 1.996

1.970  
2.201  
2.499

DATA LGR TEMP 239.21 145.50 245.40 149.20 334.07 232.12 335.70 247.40 370.00 234.50 387.60 281.20  
 CORRECTED TEMP 239.40 142.42 241.51 140.03 320.42 225.40 331.51 246.39 366.02 232.11 380.23 290.65  
 \*\*\*\*\* NUCLEAR HEATING MATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.705 3.461 2.718 2.355

9/11/67. TIME = 12.37 TO 12.44 59.0 sec. 0.00 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 26.63 IN.  
 #11 TEMP = 137.0 DEG F. MTRLT = 132.5 F. MTRLT = 137.0 F. MTL FLOW = 63.6 GPM  
 \*\*\*\*\* NUCLEAR HEATING MATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 2.723 3.461 2.718 2.355

DATA LGR TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 268.20 205.90 313.00 197.00 303.70 252.50 380.10 271.10 433.80 264.40 451.80 307.20  
 CORRECTED TEMP 203.34 203.10 304.43 198.45 369.21 244.76 376.17 269.98 427.53 260.31 441.87 306.07  
 \*\*\*\*\* NUCLEAR HEATING MATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.329 4.029 2.753 3.0351

9/11/67. TIME = 12.53 TO 13.02 59.0 sec. 5.20 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 26.64 IN.  
 #11 TEMP = 138.0 DEG F. MTRLT = 133.7 F. MTRLT = 137.0 F. MTL FLOW = 63.6 GPM  
 \*\*\*\*\* NUCLEAR HEATING MATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* INDICATED POWER \*\*\*\*\*  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 4.738 3.017 3.634  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 4.754 3.027 3.646

DATA LGR TEMP 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 244.10 211.60 321.70 202.00 408.10 265.30 404.90 284.40 496.30 279.30 485.60 322.80  
 CORRECTED TEMP 279.43 208.86 322.71 202.46 393.65 257.12 400.56 283.22 459.41 274.36 475.91 321.03

9/17/77 TIEFF = 13.00 TO 13.10 55.9 MM. 3.20 INCHES FROM FINAL IN. 510 MICRONS. RON BNK POS 26-65 N.

132-0 E. WILLOW = 63.6 GPM

• • • • • • • • • • • • • • • • •

TMPCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA 1 2 3 4 5 6 7 8 9 10 11 12  
DATA 1 2 3 4 5 6 7 8 9 10 11 12

183-12 325-6  
183-12 325-6

WELFARE MEETING RATES (AT 15/GPI) .....

TIME = 12 25 TO 13 34 52 ± 0.01  
1-20 INCHES FROM EMI IMI  
510 MICRONS. ROD BNK POS = 26.68 IN.

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## NUCLEAR MEETING NOTES (ATTACH)

**FAR CYLINDER**    **MIDDLE CYLINDER**    **NEAR CYLINDER**

2007-2008  
2008-2009  
2009-2010  
2010-2011  
2011-2012  
2012-2013  
2013-2014  
2014-2015  
2015-2016  
2016-2017  
2017-2018  
2018-2019  
2019-2020  
2020-2021  
2021-2022

9/11/2017, 11:30 AM - 11:31 AM Page 133

FIR TEMP = 136.0 CEG F. MINFLR = 134.3 F. MTRULI = 136.0 F. MT1 FLOW = 63.6 GPM

Temperature (Degrees F)      °

THEORY AND PRACTICE IN THE FIELD OF COMPUTER SECURITY

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9/12/67, TIME = 9.05 TO 9.54 00.0 MM, 45.20 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 27.79 IN.  
 RIN TEMP = 132.0 DEG F. MTINTL = 129.0 F. MTOURLT = 138.0 F. MT1 FLOW = 63.0 GPM  
 DATA LGN TEMP 138.50 141.40 137.20 136.40 136.90 135.60 136.20 135.80 136.60 135.70 136.80 136.90  
 CORRECTED TEMP 137.74 130.46 130.09 138.32 129.82 127.89 137.63 136.60 135.22 136.11 136.76 133.41  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 -0.064 .152 .129 -.044  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 -.031 -.128 -.193 -.031

9/12/67, TIME = 9.01 TO 9.10 59.3 MM, 40.00 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 27.84 IN.  
 RIN TEMP = 133.0 DEG F. MTINTL = 129.4 F. MTOURLT = 138.5 F. MT1 FLOW = 63.7 GPM  
 DATA LGN TEMP 139.30 142.70 139.30 136.70 138.20 136.10 138.30 137.40 137.90 136.60 138.10 137.70  
 CORRECTED TEMP 138.51 139.71 132.61 138.61 131.27 128.46 140.53 138.16 136.54 136.98 138.03 134.23  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 -.031 -.128 -.194 -.031

9/12/67, TIME = 9.17 TO 9.26 59.8 MM, 30.10 INCHES FROM FULL IN. 510 MICRONS. RON BNK POS = 27.84 IN.  
 RIN TEMP = 133.0 DEG F. MTINTL = 129.0 F. MTOURLT = 139.0 F. MT1 FLOW = 63.7 GPM  
 NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
 3.053 4.063 3.053 4.063 3.053 4.063 3.053 4.063 3.053 4.063 3.053 4.063

THMCPL NO 1 2 3 4 5 6 7 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \* \* \* \* \* \* \*  
 DATA LGR TEMP 143.40 145.00 147.70 138.80 148.60 141.00 149.60 144.00 146.50 138.70 147.10 146.50  
 CORRECTED TEMP 142.44 142.67 141.71 140.65 142.92 151.92 150.17 144.61 145.31 139.02 146.78 143.25  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 .119 .302 .041  
 .303 .302 .042

9/12/67. TIME = 9.33 TO 9.42 59.7 MW. 25.10 INCHES FROM FULL IN, 510 MICRONS. ROD BNK POS = 27.89 IN.  
 FIX TEMP = 133.0 DEG F. HTINLT = 130.3 F. HTOUTLT = 139.0 F. HT1 FLOW = 63.7 GPM  
 \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \* \* \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \* \* \* \* \* \* \*  
 DATA LGR TEMP 150.00 153.00 165.40 146.40 168.30 149.60 166.30 152.60 163.20 147.40 168.90 163.20  
 CORRECTED TEMP 148.82 149.55 161.31 148.02 164.99 143.76 165.80 153.01 160.15 147.49 167.99 160.38  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 .312 .562 .301  
 .565 .303 .303

9/12/67. TIME = 9.51 TO 10.00 59.6 MW. 20.20 INCHES FROM FULL IN, 510 MICRONS. ROD BNK POS = 27.94 IN.  
 FIX TEMP = 135.0 DEG F. HTINLT = 130.3 F. HTOUTLT = 138.0 F. HT1 FLOW = 63.7 GPM  
 \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \* \* \* \* \* \* \*  
 THMCPL NO 1 2 3 4 5 6 7 \* \* \* \* \* TEMPERATURE (DEGREES F) \* \* \* \* \* \* \* \* \* \* \*  
 DATA LGR TEMP 169.60 164.60 200.70 158.20 214.70 174.20 213.60 179.00 209.20 164.60 218.40 198.00  
 CORRECTED TEMP 167.84 160.80 194.84 159.46 208.3A 171.00 210.46 179.33 204.79 164.22 216.66 196.69  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 1.007 .998 1.014  
 1.004 .950 1.004  
 .956 .956

9/12/67, TIME = 10.07 TO 10.16 59.6 MW, 18.10 INCHES FROM FULL IN., 510 MICRONS, ROD BNK POS = 27.99 IN.  
 FIX TEMP = 135.0 DEG F, HTINLT = 131.3 F, HTOUTLT = 138.0 F, HT1 FLOW = 63.5 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 182.50 172.40 221.80 166.30 243.50 186.30 240.20 194.90 242.90 180.40 255.80 217.50  
 CORRECTED TEMP 181.10 168.70 215.17 167.31 236.08 182.35 235.84 194.65 239.27 180.12 253.32 216.42  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 1.393 1.258 1.524 1.534  
 1.402 1.266

9/13/67, TIME = 9.10 TO 9.19 60.0 MW, 44.90 INCHES FROM FULL IN., 510 MICRONS, ROD BNK POS = 29.69 IN.  
 FIX TEMP = 135.0 DEG F, HTINLT = 129.9 F, HTOUTLT = 141.0 F, HT1 FLOW = 64.0 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 139.50 142.20 138.30 138.20 138.90 137.80 138.10 137.50 137.90 137.90 139.30 139.00  
 CORRECTED TEMP 138.70 139.23 131.31 140.07 132.06 130.38 139.41 138.26 136.54 138.25 139.19 135.56  
 \*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
 \*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
 \*\*\*\*\* NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER \*\*\*\*\*  
 -0.050 0.139 -0.106 0.139

9/13/67, TIME = 9.27 TO 9.36 60.0 MW, 39.80 INCHES FROM FULL IN., 510 MICRONS, ROD BNK POS = 29.79 IN.  
 FIX TEMP = 134.0 DEG F, HTINLT = 130.2 F, HTOUTLT = 140.0 F, HT1 FLOW = 64.1 GPM  
 \*  
 TMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
 DATA LGR TEMP 140.00 144.00 140.50 139.10 140.50 138.30 140.50 139.00 139.20 137.40 139.80 139.50

CORRECTED TEMP 140.04 140.95 133.74 140.94 133.85 130.95 141.66 139.73 137.87 137.76 139.68 136.08  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER FAR CYLINDER  
-.027 -.126 -.027 -.177 -.126

9/13/67, TIME = 9.43 TO 9.52 60.2 MW, 30.00 INCHES FROM FULL IN. 510 MICRONS, RDN BNK POS = 29.79 IN.  
FIX TEMP = 134.0 DEG F, HTINLT = 131.1 F, HTOUTLT = 140.0 F, HT1 FLOW = 64.1 GPM  
\*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 145.60 148.90 150.70 141.60 150.40 142.80 150.40 145.30 148.80 142.20 149.60 148.20  
CORRECTED TEMP 144.55 145.63 145.04 143.36 144.94 136.05 150.92 145.88 147.65 142.43 149.41 145.00  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER FAR CYLINDER  
.013 .309 .108 .013 .307 .013

9/13/67, TIME = 10.29 TO 10.38 60.0 MW, 25.00 INCHES FROM FULL IN, 510 MICRONS, RDN BNK POS = 29.92 IN.  
FIX TEMP = 135.0 DEG F, HTINLT = 132.1 F, HTOUTLT = 142.0 F, HT1 FLOW = 64.1 GPM  
\*  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 153.20 156.50 167.30 148.00 169.40 151.70 169.80 156.40 165.90 149.70 170.80 164.40  
CORRECTED TEMP 151.92 152.89 163.42 149.57 166.22 146.14 169.08 156.73 162.74 149.73 169.84 161.61  
\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER FAR CYLINDER  
.309 .559 .269 .309 .559 .269

9/13/67. TIME = 10.45 TO 10.54 59.0 MM. 20.00 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 29.98 IN.

PLX TEMP = 136.0 DEG F. MTINLT = 132.5 F. MTOUTLT = 142.0 F. MT1 FLOW = 64.1 GPM  
THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 172.00 168.20 203.50 161.50 217.10 175.10 214.20 180.90 213.00 168.40 224.50 200.60  
CORRECTED TEMP 170.17 164.44 197.35 162.66 210.66 171.82 211.01 181.19 208.65 167.92 222.60 199.32

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.0360 1.0260 1.0390 1.0270 1.0340 1.0240 1.0300 1.0230 1.0310 1.0210 1.0370 1.0200

9/13/67. TIME = 11.01 TO 11.10 59.7 MM. 18.00 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 30.08 IN.

PLX TEMP = 13.0 DEG F. MTINLT = 132.5 F. MTOUTLT = 142.0 F. MT1 FLOW = 64.2 GPM

THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 185.10 175.10 224.10 167.80 244.70 188.50 243.20 197.00 245.60 182.80 258.30 219.40  
CORRECTED TEMP 183.62 171.76 217.56 168.76 237.22 184.15 238.89 196.70 242.01 182.66 255.75 218.32

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*  
\*\*\*\*\* AT INDICATED POWER \*\*\*\*\*  
\*\*\*\*\* NORMALIZED TO 60 MW \*\*\*\*\*  
NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER NEAR CYLINDER MIDDLE CYLINDER FAR CYLINDER  
1.540 1.417 1.547 1.257 1.410 1.263

9/13/67. TIME = 11.17 TO 11.24 59.8 MM. 18.29 INCHES FROM FULL IN. 510 MICRONS, ROD BNK POS = 30.09 IN.

PLX TEMP = 138.0 DEG F. MTINLT = 132.2 F. MTOUTLT = 142.0 F. MT1 FLOW = 64.1 GPM

THMCPL NO 1 2 3 4 5 6 7 8 9 10 11 12  
DATA LGR TEMP 201.10 181.70 242.40 174.20 271.60 201.50 269.40 213.40 278.40 196.10 293.70 236.90  
CORRECTED TEMP 198.98 178.66 236.87 175.27 262.84 195.95 265.54 212.82 275.71 195.18 290.25 236.18

\*\*\*\*\* NUCLEAR HEATING RATES (WATTS/GM) \*\*\*\*\*

9/13/67. TIME = 11.33 TO 11.42 59.8 sec. 15.00 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 30.18 IN.  
F1: TEMP = 130.0 DEG F. RTINT = 133.5 F. RTOUTL = 142.0 F. RT1 FLOW = 64.2 GPM  
•  
TEMP, NC DATA LOG TEMP 211.40 186.30 258.10 181.10 295.00 212.60 249.50 223.60 308.00 209.50 324.50 252.60  
CORRECTED TEMP 208.85 183.54 253.19 182.17 285.13 205.96 285.96 222.66 305.21 208.28 319.39 251.94

9/13/67. TIME = 11.33 TO 11.42 59.9 sec. 14.98 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 30.23 IN.  
F1: TEMP = 130.0 DEG F. RTINT = 133.8 F. RTOUTL = 142.0 F. RT1 FLOW = 64.1 GPM  
•  
TEMP, NC DATA LOG TEMP 223.50 192.80 208.40 183.90 312.10 219.80 308.60 236.10 332.20 219.10 347.40 262.70  
CORRECTED TEMP 220.44 189.38 203.90 185.10 300.74 212.91 304.78 233.15 328.50 217.33 341.62 262.08

9/13/67. TIME = 11.49 TO 11.58 59.9 sec. 14.98 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 30.27 IN.  
F1: TEMP = 130.0 DEG F. RTINT = 133.8 F. RTOUTL = 142.0 F. RT1 FLOW = 64.1 GPM  
•  
TEMP, NC DATA LOG TEMP 211.40 186.30 258.10 181.10 295.00 212.60 249.50 223.60 308.00 209.50 324.50 252.60  
CORRECTED TEMP 208.85 183.54 253.19 182.17 285.13 205.96 285.96 222.66 305.21 208.28 319.39 251.94

9/13/67. TIME = 11.33 TO 11.42 59.8 sec. 15.00 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 30.18 IN.  
F1: TEMP = 130.0 DEG F. RTINT = 133.5 F. RTOUTL = 142.0 F. RT1 FLOW = 64.2 GPM  
•  
TEMP, NC DATA LOG TEMP 211.40 186.30 258.10 181.10 295.00 212.60 249.50 223.60 308.00 209.50 324.50 252.60  
CORRECTED TEMP 208.85 183.54 253.19 182.17 285.13 205.96 285.96 222.66 305.21 208.28 319.39 251.94

9/13/67. TIME = 11.33 TO 11.42 59.9 sec. 14.98 INCHES FROM FULL IN. 510 MICRONS. RDN BNK POS = 30.23 IN.  
F1: TEMP = 130.0 DEG F. RTINT = 133.8 F. RTOUTL = 142.0 F. RT1 FLOW = 64.1 GPM  
•  
TEMP, NC DATA LOG TEMP 211.40 186.30 258.10 181.10 295.00 212.60 249.50 223.60 308.00 209.50 324.50 252.60  
CORRECTED TEMP 208.85 183.54 253.19 182.17 285.13 205.96 285.96 222.66 305.21 208.28 319.39 251.94

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PLATE 10.—A. *Leptostoma* sp. (holotype); B. *Leptostoma* sp. (paratype).

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THE JOURNAL OF CLIMATE

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510 TICKETS. NON TICKETS = 3043 IN.

2020-2021  
2021-2022  
2022-2023  
2023-2024

**CORRECTED TEST**      **2000-0-69**      **201-0-88**      **312-2-1**

0113747. There is also 0.300 m. 8.40 m. 13.19 g. 90.4 m. 318 microns. MUL HAN PUS = 30.3A IN.

01/12/07, 11:26 = 10.11 70 10.36 59.8 sec. 0.00 Incrds roro fuel ltr. \$10 incrds roro fuel ltr. \$0.00 roro roro = 39.38 ltr.

01/12/07, 11:26 = 10.20 70 10.36 59.8 sec. 0.00 Incrds roro fuel ltr. \$10 incrds roro fuel ltr. \$0.00 roro roro = 39.38 ltr.

DATA LOG TIME 200.00 211.70 229.40 260.30 413.00 299.00 400.00 299.00 401.00 291.00 402.00 292.00 403.00 293.00 404.00 294.00 405.00 295.00 406.00 296.00 407.00 297.00 408.00 298.00 409.00 299.00 410.00 300.00 411.00 301.00 412.00 302.00 413.00 303.00 414.00 304.00 415.00 305.00 416.00 306.00 417.00 307.00 418.00 308.00 419.00 309.00 420.00 310.00 421.00 311.00 422.00 312.00 423.00 313.00 424.00 314.00 425.00 315.00 426.00 316.00 427.00 317.00 428.00 318.00 429.00 319.00 430.00 320.00 431.00 321.00 432.00 322.00 433.00 323.00 434.00 324.00 435.00 325.00 436.00 326.00 437.00 327.00 438.00 328.00 439.00 329.00 440.00 330.00 441.00 331.00 442.00 332.00 443.00 333.00 444.00 334.00 445.00 335.00 446.00 336.00 447.00 337.00 448.00 338.00 449.00 339.00 450.00 340.00 451.00 341.00 452.00 342.00 453.00 343.00 454.00 344.00 455.00 345.00 456.00 346.00 457.00 347.00 458.00 348.00 459.00 349.00 460.00 350.00 461.00 351.00 462.00 352.00 463.00 353.00 464.00 354.00 465.00 355.00 466.00 356.00 467.00 357.00 468.00 358.00 469.00 359.00 470.00 360.00 471.00 361.00 472.00 362.00 473.00 363.00 474.00 364.00 475.00 365.00 476.00 366.00 477.00 367.00 478.00 368.00 479.00 369.00 480.00 370.00 481.00 371.00 482.00 372.00 483.00 373.00 484.00 374.00 485.00 375.00 486.00 376.00 487.00 377.00 488.00 378.00 489.00 379.00 490.00 380.00 491.00 381.00 492.00 382.00 493.00 383.00 494.00 384.00 495.00 385.00 496.00 386.00 497.00 387.00 498.00 388.00 499.00 389.00 500.00 390.00 501.00 391.00 502.00 392.00 503.00 393.00 504.00 394.00 505.00 395.00 506.00 396.00 507.00 397.00 508.00 398.00 509.00 399.00 510.00 400.00 511.00 401.00 512.00 402.00 513.00 403.00 514.00 404.00 515.00 405.00 516.00 406.00 517.00 407.00 518.00 408.00 519.00 409.00 520.00 410.00 521.00 411.00 522.00 412.00 523.00 413.00 524.00 414.00 525.00 415.00 526.00 416.00 527.00 417.00 528.00 418.00 529.00 419.00 530.00 420.00 531.00 421.00 532.00 422.00 533.00 423.00 534.00 424.00 535.00 425.00 536.00 426.00 537.00 427.00 538.00 428.00 539.00 429.00 540.00 430.00 541.00 431.00 542.00 432.00 543.00 433.00 544.00 434.00 545.00 435.00 546.00 436.00 547.00 437.00 548.00 438.00 549.00 439.00 550.00 440.00 551.00 441.00 552.00 442.00 553.00 443.00 554.00 444.00 555.00 445.00 556.00 446.00 557.00 447.00 558.00 448.00 559.00 449.00 560.00 450.00 561.00 451.00 562.00 452.00 563.00 453.00 564.00 454.00 565.00 455.00 566.00 456.00 567.00 457.00 568.00 458.00 569.00 459.00 570.00 460.00 571.00 461.00 572.00 462.00 573.00 463.00 574.00 464.00 575.00 465.00 576.00 466.00 577.00 467.00 578.00 468.00 579.00 469.00 580.00 470.00 581.00 471.00 582.00 472.00 583.00 473.00 584.00 474.00 585.00 475.00 586.00 476.00 587.00 477.00 588.00 478.00 589.00 479.00 590.00 480.00 591.00 481.00 592.00 482.00 593.00 483.00 594.00 484.00 595.00 485.00 596.00 486.00 597.00 487.00 598.00 488.00 599.00 489.00 600.00 490.00 601.00 491.00 602.00 492.00 603.00 493.00 604.00 494.00 605.00 495.00 606.00 496.00 607.00 497.00 608.00 498.00 609.00 499.00 610.00 500.00 611.00 501.00 612.00 502.00 613.00 503.00 614.00 504.00 615.00 505.00 616.00 506.00 617.00 507.00 618.00 508.00 619.00 509.00 620.00 510.00 621.00 511.00 622.00 512.00 623.00 513.00 624.00 514.00 625.00 515.00 626.00 516.00 627.00 517.00 628.00 518.00 629.00 519.00 630.00 520.00 631.00 521.00 632.00 522.00 633.00 523.00 634.00 524.00 635.00 525.00 636.00 526.00 637.00 527.00 638.00 528.00 639.00 529.00 640.00 530.00 641.00 531.00 642.00 532.00 643.00 533.00 644.00 534.00 645.00 535.00 646.00 536.00 647.00 537.00 648.00 538.00 649.00 539.00 650.00 540.00 651.00 541.00 652.00 542.00 653.00 543.00 654.00 544.00 655.00 545.00 656.00 546.00 657.00 547.00 658.00 548.00 659.00 549.00 660.00 550.00 661.00 551.00 662.00 552.00 663.00 553.00 664.00 554.00 665.00 555.00 666.00 556.00 667.00 557.00 668.00 558.00 669.00 559.00 670.00 560.00 671.00 561.00 672.00 562.00 673.00 563.00 674.00 564.00 675.00 565.00 676.00 566.00 677.00 567.00 678.00 568.00 679.00 569.00 680.00 570.00 681.00 571.00 682.00 572.00 683.00 573.00 684.00 574.00 685.00 575.00 686.00 576.00 687.00 577.00 688.00 578.00 689.00 579.00 690.00 580.00 691.00 581.00 692.00 582.00 693.00 583.00 694.00 584.00 695.00 585.00 696.00 586.00 697.00 587.00 698.00 588.00 699.00 589.00 700.00 590.00 701.00 591.00 702.00 592.00 703.00 593.00 704.00 594.00 705.00 595.00 706.00 596.00 707.00 597.00 708.00 598.00 709.00 599.00 710.00 600.00 711.00 601.00 712.00 602.00 713.00 603.00 714.00 604.00 715.00 605.00 716.00 606.00 717.00 607.00 718.00 608.00 719.00 609.00 720.00 610.00 721.00 611.00 722.00 612.00 723.00 613.00 724.00 614.00 725.00 615.00 726.00 616.00 727.00 617.00 728.00 618.00 729.00 619.00 730.00 620.00 731.00 621.00 732.00 622.00 733.00 623.00 734.00 624.00 735.00 625.00 736.00 626.00 737.00 627.00 738.00 628.00 739.00 629.00 740.00 630.00 741.00 631.00 742.00 632.00 743.00 633.00 744.00 634.00 745.00 635.00 746.00 636.00 747.00 637.00 748.00 638.00 749.00 639.00 750.00 640.00 751.00 641.00 752.00 642.00 753.00 643.00 754.00 644.00 755.00 645.00 756.00 646.00 757.00 647.00 758.00 648.00 759.00 649.00 760.00 650.00 761.00 651.00 762.00 652.00 763.00 653.00 764.00 654.00 765.00 655.00 766.00 656.00 767.00 657.00 768.00 658.00 769.00 659.00 770.00 660.00 771.00 661.00 772.00 662.00 773.00 663.00 774.00 664.00 775.00 665.00 776.00 666.00 777.00 667.00 778.00 668.00 779.00 669.00 780.00 670.00 781.00 671.00 782.00 672.00 783.00 673.00 784.00 674.00 785.00 675.00 786.00 676.00 787.00 677.00 788.00 678.00 789.00 679.00 790.00 680.00 791.00 681.00 792.00 682.00 793.00 683.00 794.00 684.00 795.00 685.00 796.00 686.00 797.00 687.00 798.00 688.00 799.00 689.00 800.00 690.00 801.00 691.00 802.00 692.00 803.00 693.00 804.00 694.00 805.00 695.00 806.00 696.00 807.00 697.00 808.00 698.00 809.00 699.00 810.00 700.00 811.00 701.00 812.00 702.00 813.00 703.00 814.00 704.00 815.00 705.00 816.00 706.00 817.00 707.00 818.00 708.00 819.00 709.00 820.00 710.00 821.00 711.00 822.00 712.00 823.00 713.00 824.00 714.00 825.00 715.00 826.00 716.00 827.00 717.00 828.00 718.00 829.00 719.00 830.00 720.00 831.00 721.00 832.00 722.00 833.00 723.00 834.00 724.00 835.00 725.00 836.00 726.00 837.00 727.00 838.00 728.00 839.00 729.00 840.00 730.00 841.00 731.00 842.00 732.00 843.00 733.00 844.00 734.00 845.00 735.00 846.00 736.00 847.00 737.00 848.00 738.00 849.00 739.00 850.00 740.00 851.00 741.00 852.00 742.00 853.00 743.00 854.00 744.00 855.00 745.00 856.00 746.00 857.00 747.00 858.00 748.00 859.00 749.00 860.00 750.00 861.00 751.00 862.00 752.00 863.00 753.00 864.00 754.00 865.00 755.00 866.00 756.00 867.00 757.00 868.00 758.00 869.00 759.00 870.00 760.00 871.00 761.00 872.00 762.00 873.00 763.00 874.00 764.00 875.00 765.00 876.00 766.00 877.00 767.00 878.00 768.00 879.00 769.00 880.00 770.00 881.00 771.00 882.00 772.00 883.00 773.00 884.00 774.00 885.00 775.00 886.00 776.00 887.00 777.00 888.00 778.00 889.00 779.00 890.00 780.00 891.00 781.00 892.00 782.00 893.00 783.00 894.00 784.00 895.00 785.00 896.00 786.00 897.00 787.00 898.00 788.00 899.00 789.00 900.00 790.00 901.00 791.00 902.00 792.00 903.00 793.00 904.00 794.00 905.00 795.00 906.00 796.00 907.00 797.00 908.00 798.00 909.00 799.00 910.00 800.00 911.00 801.00 912.00 802.00 913.00 803.00 914.00 804.00 915.00 805.00 916.00 806.00 917.00 807.00 918.00 808.00 919.00 809.00 920.00 810.00 921.00 811.00 922.00 812.00 923.00 813.00 924.00 814.00 925.00 815.00 926.00 816.00 927.00 817.00 928.00 818.00 929.00 819.00 930.00 820.00 931.00 821.00 932.00 822.00 933.00 823.00 934.00 824.00 935.00 825.00 936.00 826.00 937.00 827.00 938.00 828.00 939.00 829.00 940.00 830.00 941.00 831.00 942.00 832.00 943.00 833.00 944.00 834.00 945.00 835.00 946.00 836.00 947.00 837.00 948.00 838.00 949.00 839.00 950.00 840.00 951.00 841.00 952.00 842.00 953.00 843.00 954.00 844.00 955.00 845.00 956.00 846.00 957.00 847.00 958.00 848.00 959.00 849.00 960.00 850.00 961.00 851.00 962.00 852.00 963.00 853.00 964.00 854.00 965.00 855.00 966.00 856.00 967.00 857.00 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1103.00 993.00 1104.00 994.00 1105.00 995.00 1106.00 996.00 1107.00 997.00 1108.00 998.00 1109.00 999.00 1110.00 1000.00 1111.00 1001.00 1112.00 1002.00 1113.00 1003.00 1114.00 1004.00 1115.00 1005.00 1116.00 1006.00 1117.00 1007.00 1118.00 1008.00 1119.00 1009.00 1120.00 1010.00 1121.00 1011.00 1122.00 1012.00 1123.00 1013.00 1124.00 1014.00 1125.00 1015.00 1126.00 1016.00 1127.00 1017.00 1128.00 1018.00 1129.00 1019.00 1130.00 1020.00 1131.00 1021.00 1132.00 1022.00 1133.00 1023.00 1134.00 1024.00 1135.00 1025.00 1136.00 1026.00 1137.00 1027.00 1138.00 1028.00 1139.00 1029.00 1140.00 1030.00 1141.00 1031.00 1142.00 1032.00 114

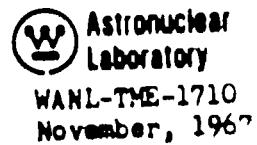


TABLE I  
Explanation of Data Logger Printout

<u>Column(s)</u>	<u>Parameter Description</u>	<u>Units</u>
32	Core Inlet Temperature	°F
33	Core Outlet Temperature	°F
34 - 38	Shim Rod Bank Position, Rods 1 - 5	Inches
39 - 41	Shim Rod Bank Position, Rods 6 - 8	Inches
42 & 43	Regulator Rod Positions, Rods 1 & 2	%
44 - 53	Calorimeter Temperatures	°F
44 & 46	Far* Calorimeter, Hot End Thermocouples	°F
45 & 47	Far* Calorimeter, Cold End Thermocouples	°F
48 & 50	Middle* Calorimeter, Hot End Thermocouples	°F
49 & 51	Middle* Calorimeter, Cold End Thermocouples	°F
52 & 54	Near* Calorimeter, Hot End Thermocouples	°F
53 & 55	Near* Calorimeter, Cold End Thermocouples	°F
56 - 59	Calorimeter Container Temperature	°F
59	HT-1 Outlet Temperature	°F
60	HT-1 Inlet Temperature	°F
61	HT-1 Flow	GPM
62, 64, ..., 64	Average Temperature From Each Calorimeter Thermocouple °F	
63, 65, ..., 65	Standard Deviation From Mean of Each Temperature	°F

\* With Respect to Reactor Core.

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 November, 1967

TABLE II  
TOSS Model Node Dimensions

<u>Node(s)</u>	<u>Outside Radius (Inches)</u>	<u>Inside Radius (Inches)</u>	<u>Length (Inches)</u>
1	0.197	0	0.03
2-5, 9, 10, 11	0.197	0	0.02
6-8	0.197	0	0.77
12	0.197	0	0.21
13	0.197	0	0.50
21	0.197	0	0.002
50	0.062	0	0.50
51 & 71	0.197	0.062	0.50
32 & 52	0.312	0.197	0.50
33 & 53 & 73	0.437	0.312	0.50
34 & 54	0.562	0.437	0.50
75 & 55 & 75	0.687	0.562	0.50
36 & 56	0.812	0.687	0.50
17 & 57 & 77	0.937	0.812	0.50
38 & 58	1.30	0.937	0.50
19 & 59	1.80	1.30	0.50
40 & 60	2.30	1.80	0.50
41 & 61	2.80	2.30	0.50
42 & 62	3.3125	2.80	0.50

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November, 1967

TABLE III  
Aluminum Thermal Conductivity As  
A Function of Temperature

<u>Temperature (°K)</u>	<u>Thermal Conductivity (calories/sec-cm-°K)</u>
200	0.566
250	0.561
273	0.563
300	0.566
350	0.573
400	0.573
500	0.573
600	0.573
700	0.539
800	0.525
900	0.508

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 November, 1967

**TABLE IV**  
**Relationship Between Nuclear Heating**  
**and Calorimeter  $\Delta T$  From**  
**TOSS Temperature Distribution**

Range Of Heating Rates (watts/gram)	Relationship Between Nuclear Heating Rate and Calorimeter $\Delta T$ (watts/gm per °R of $\Delta T$ ) At Indicated Bulk Cooling Water Temp. (°F)			
	120	125	130	135
0.2 < H < 1	.02626	.02624	.02595	.02592
1 < H < 3	.02613	.02641	.02598	.02615
3 < H < 5	.02627	.02565	.02598	.02596
5 < H < 6	.02513	.02595	.02611	.02581
6 < H < 7	.02550	.02527	.02548	.02611

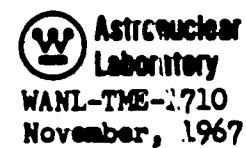


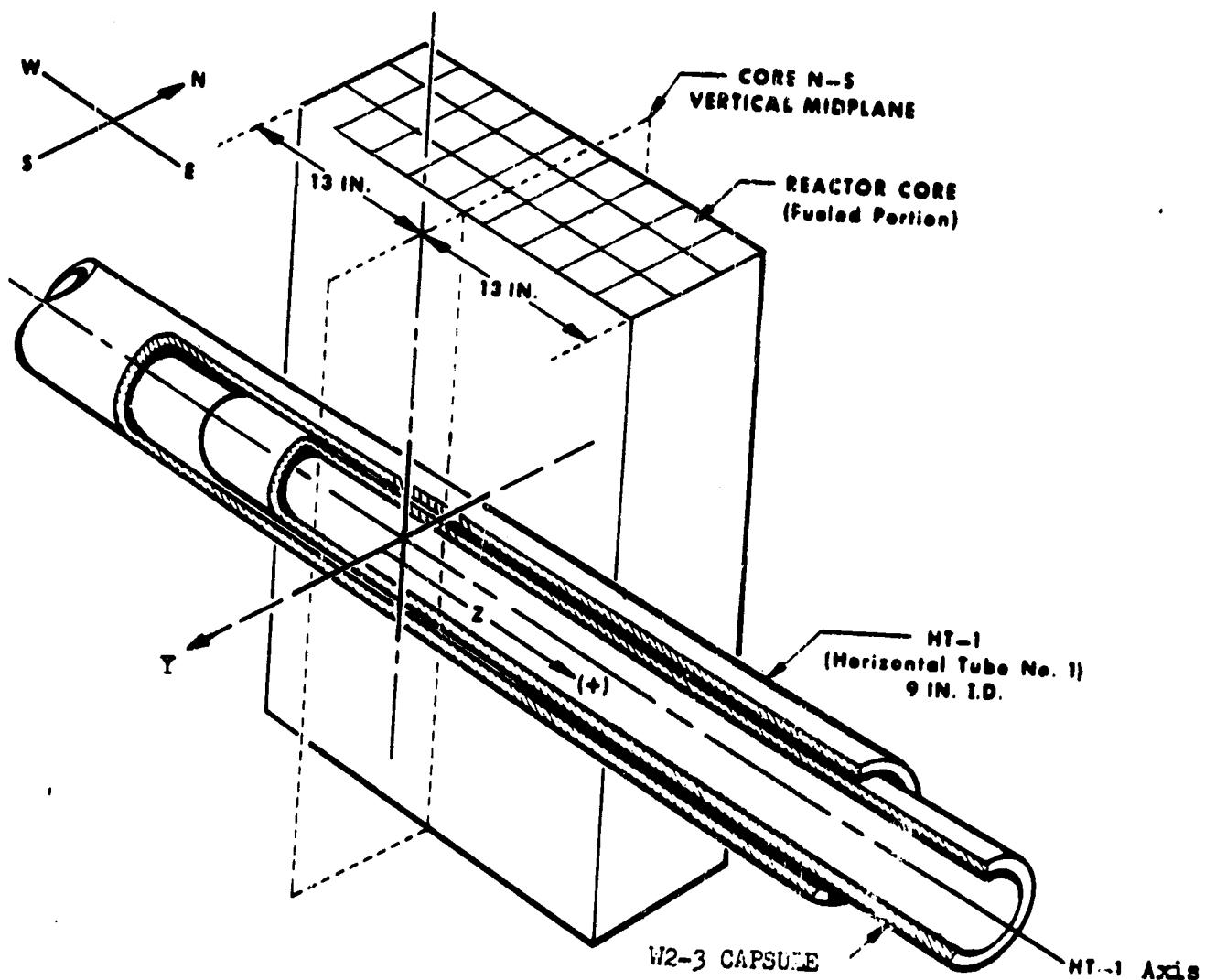
TABLE V  
Thermocouple Resistance Measurements

Thermocouple	Resistance:			Difference (ohms)
	From Chromel to Alumel (ohms)	Alumel to Ground	Plus Chromel to Ground (ohms)	
1	441.5	442.9		1.4
2	446.2	448.4		2.2
3	437.2	453.		15.8
4	431.3	432.7		1.4
5	433.	437.9		4.9
6	431.9	433.		1.1
7	430.	438.1		8.1
8	425.3	426.7		1.4
9	442.1	446.1		4.0
10	432.6	434.4		1.6
11	428.1	459.3		31.2
12	437.	444.2		7.2

TABLE VI  
 Calorimeter Accuracy  
 At The 95% Confidence Limit

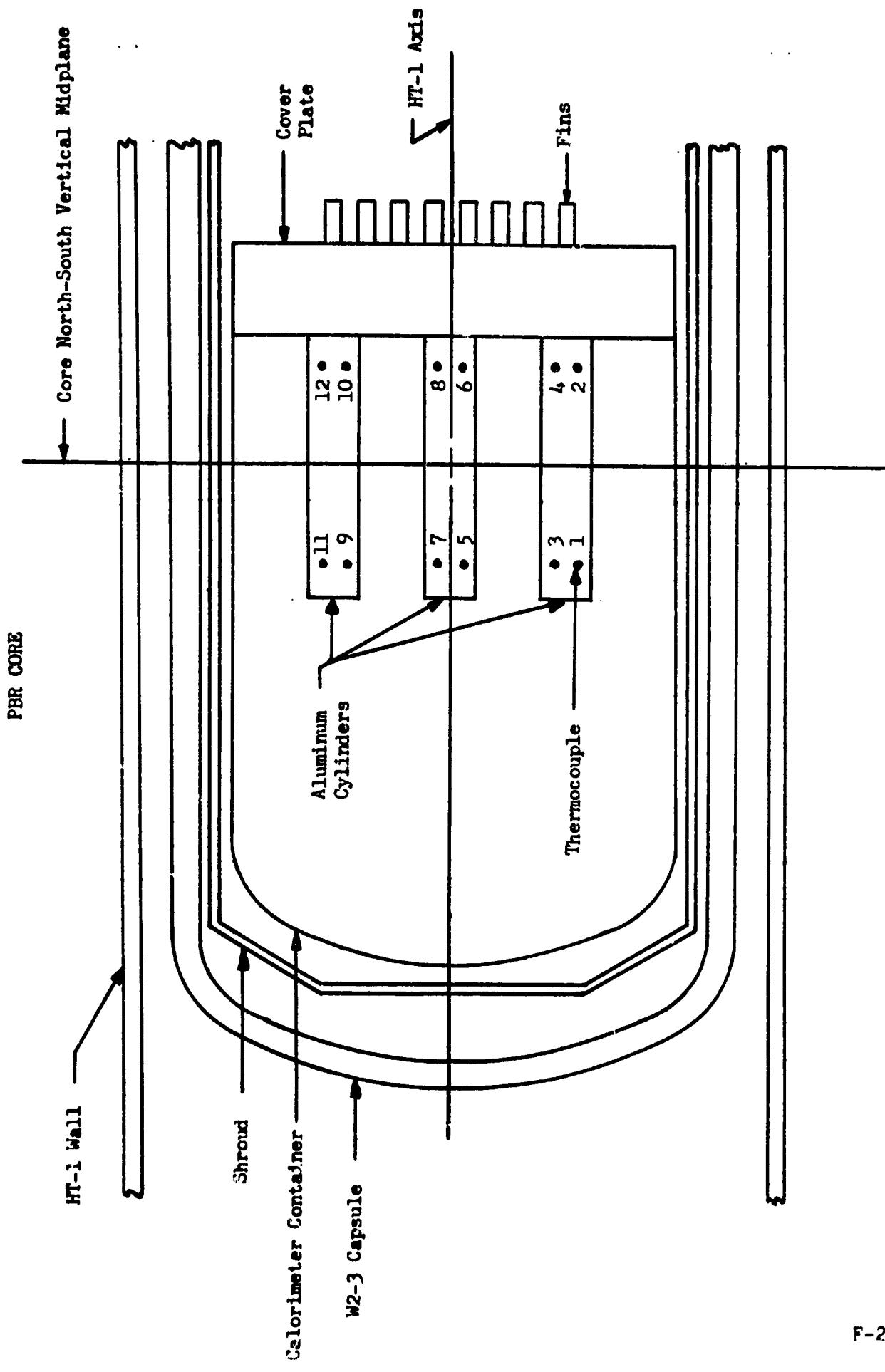
Nuclear Heat Generation Rate Measurement Uncertainties ( $\pm\%$ ),  
As A Result of Uncertainties in Each of the Indicated Parameters

Heat Generation Rate (watts/gm)	7	6	5	3	1	.2
Spatial Heating Distribution	0.681	0.702	0.948	0.903	0.526	6.18
Air Pressure in Calorimeter Container			negligible			
Emissivity of Aluminum	3.72	3.13	2.65	2.06	1.92	1.18
Thermal Conductivity of Aluminum	2.50	2.39	2.52	3.08	1.87	6.85
Distance Between T/C's	0.410	0.410	0.411	0.415	0.421	0.461
Thermocouple Calibration	0.975	1.11	1.34	2.23	6.70	33.5
Data Logger	3.18	3.72	4.46	7.44	22.3	111.2
Reactor Power	1.0	1.0	1.0	1.0	1.0	1.0
Calorimeter Cylinder Position	2.3	2.3	2.3	2.3	2.3	2.3
Combined Calorimeter Accuracy	6.16	6.12	6.53	9.00	23.6	117.



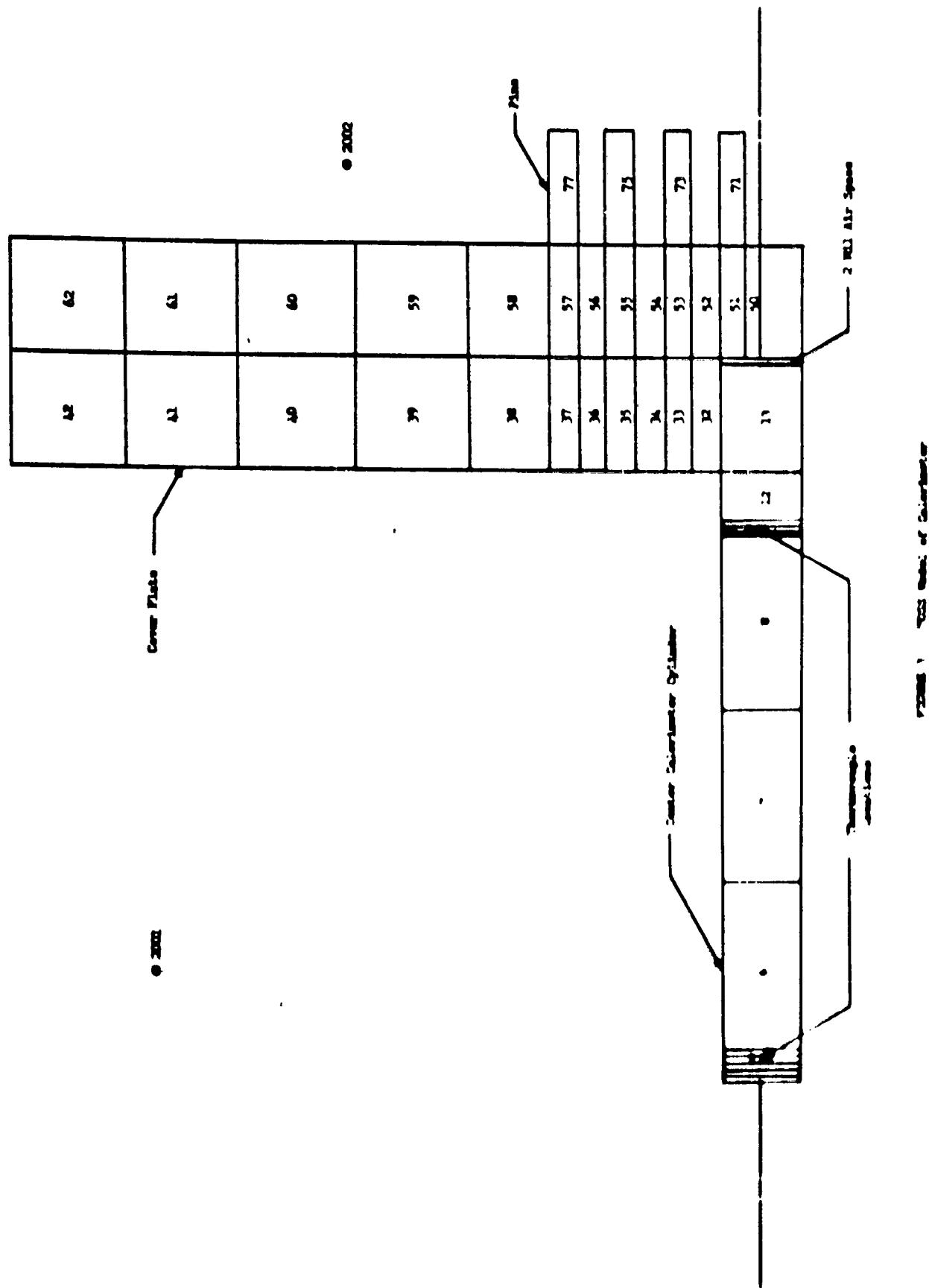
IRRADIATION TEST SYSTEM  
PLUM BROOK REACTOR - SANDUSKY, OHIO

FIGURE 1



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FIGURE 2 Calorimeter Assembly



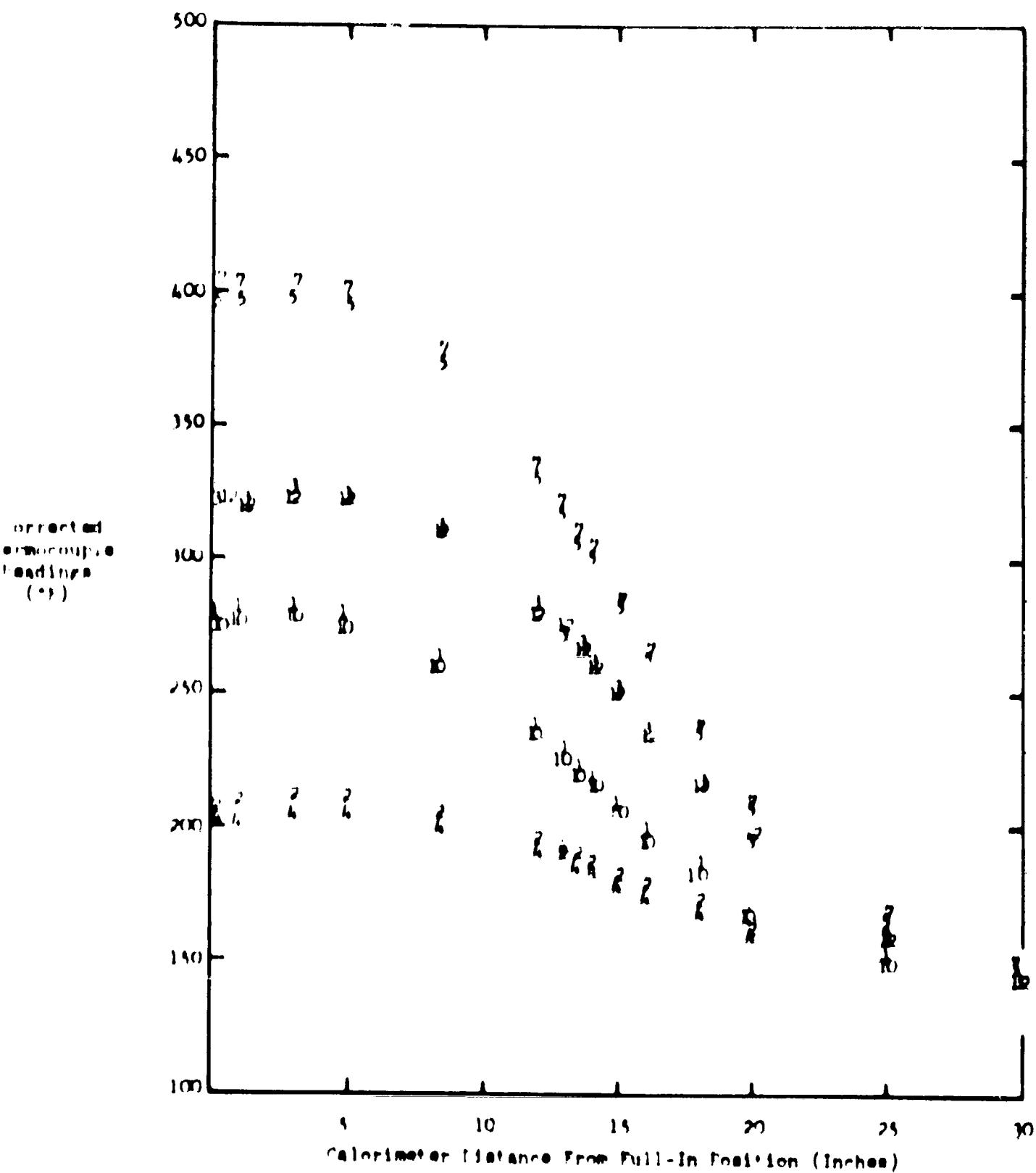


FIGURE 4. Corrected Thermocouple Readings As A Function of Calorimeter Position on September 11 (Thermocouples 1, 2, 3, 4, 5, 7, 10, 12).

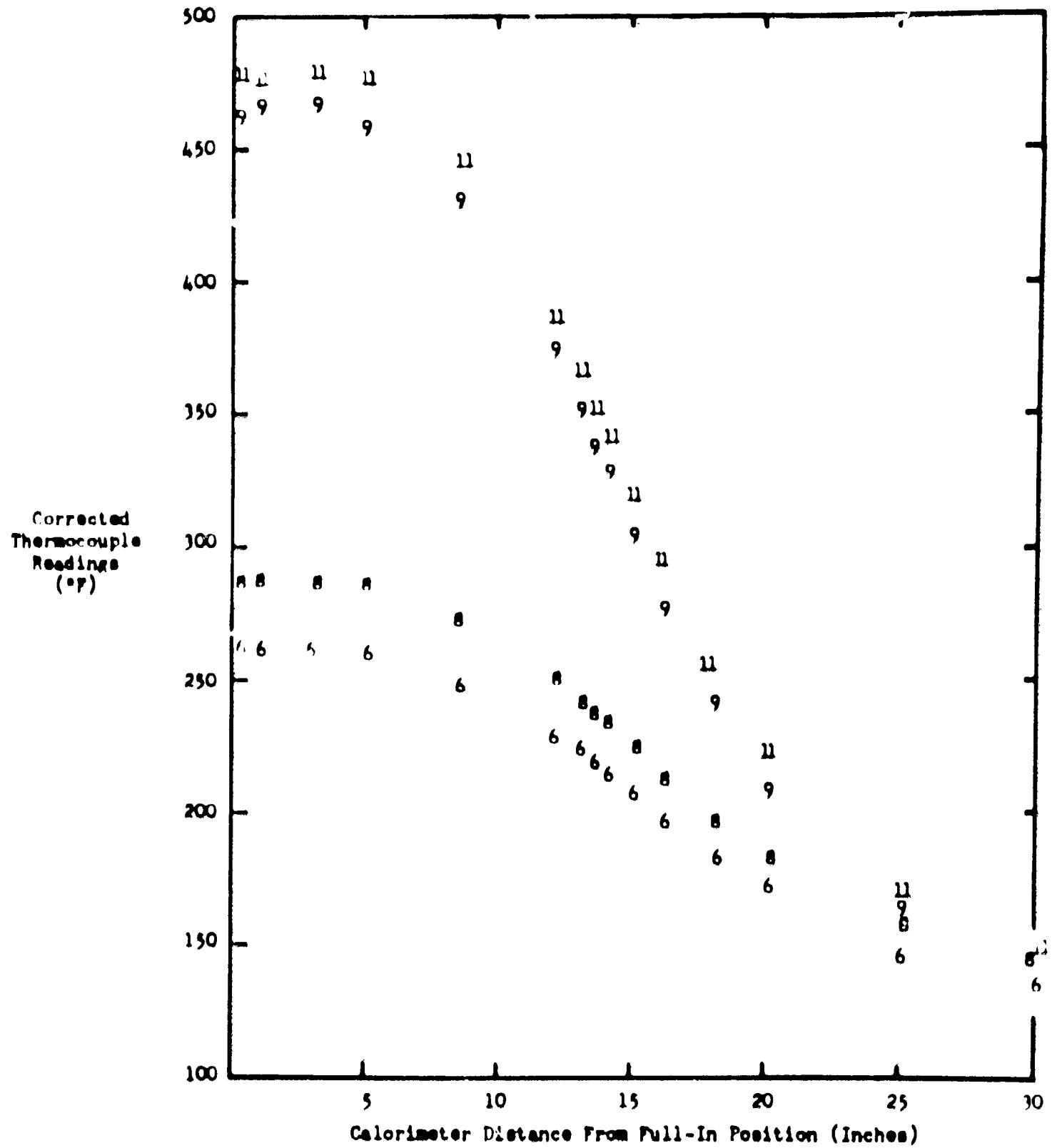


FIGURE 5 Corrected Thermocouple Readings As A Function of Calorimeter Position On September 13 (Thermocouples 6, 8, 9, 11)

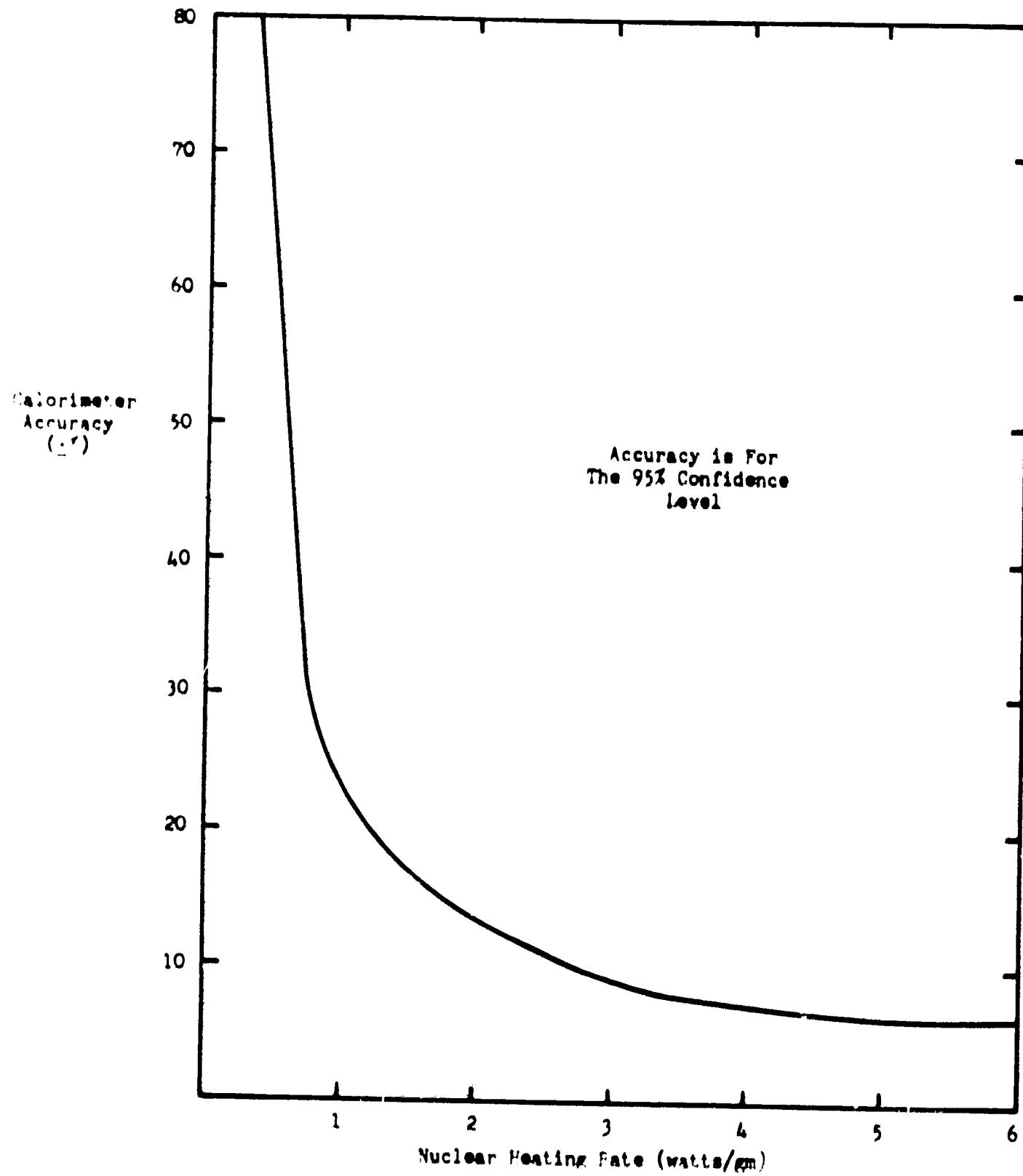


FIGURE 6 Calorimeter Accuracy Vs. Heating Rate

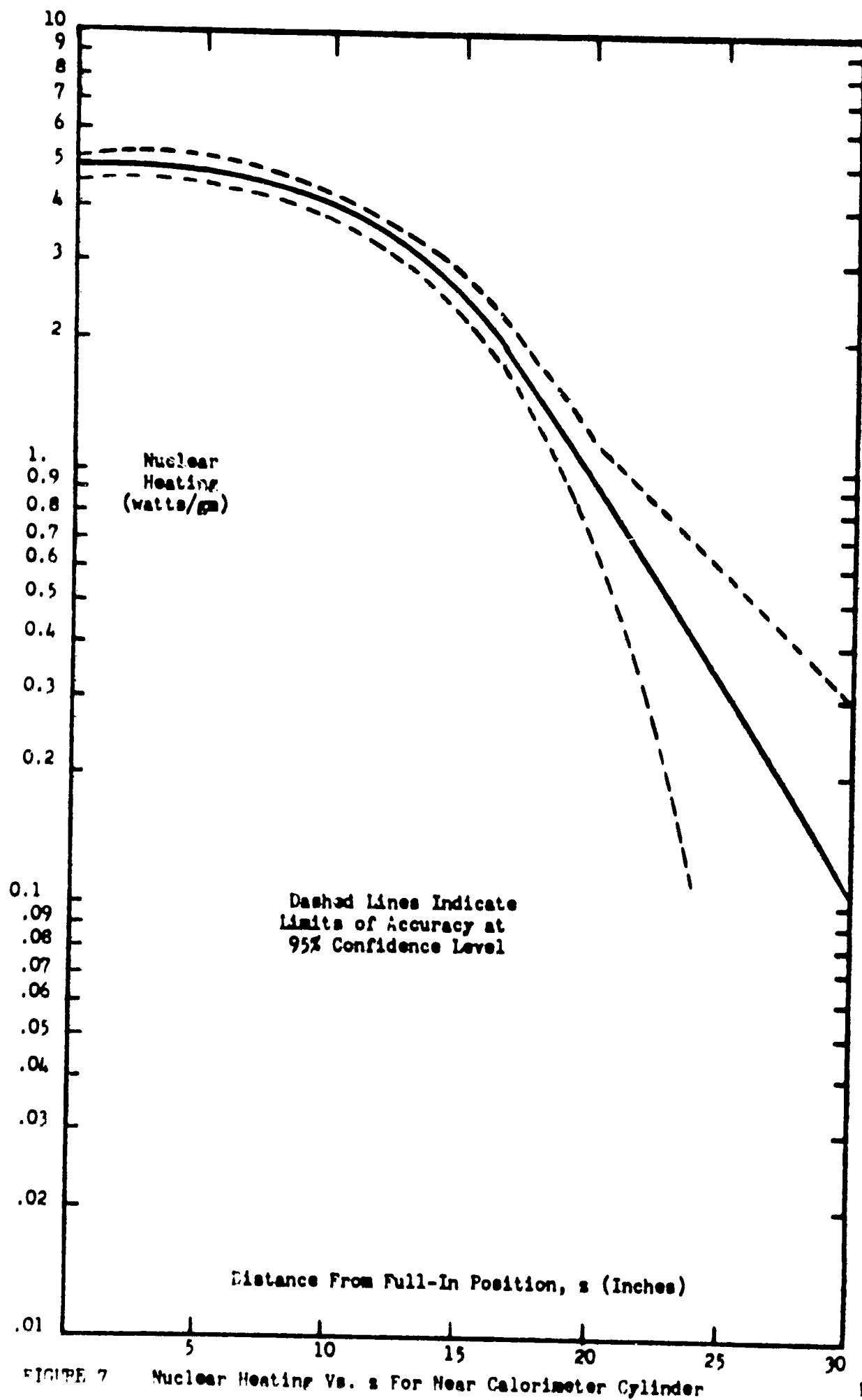


FIGURE 7 Nuclear Heating Vs.  $z$  For Near Calorimeter Cylinder

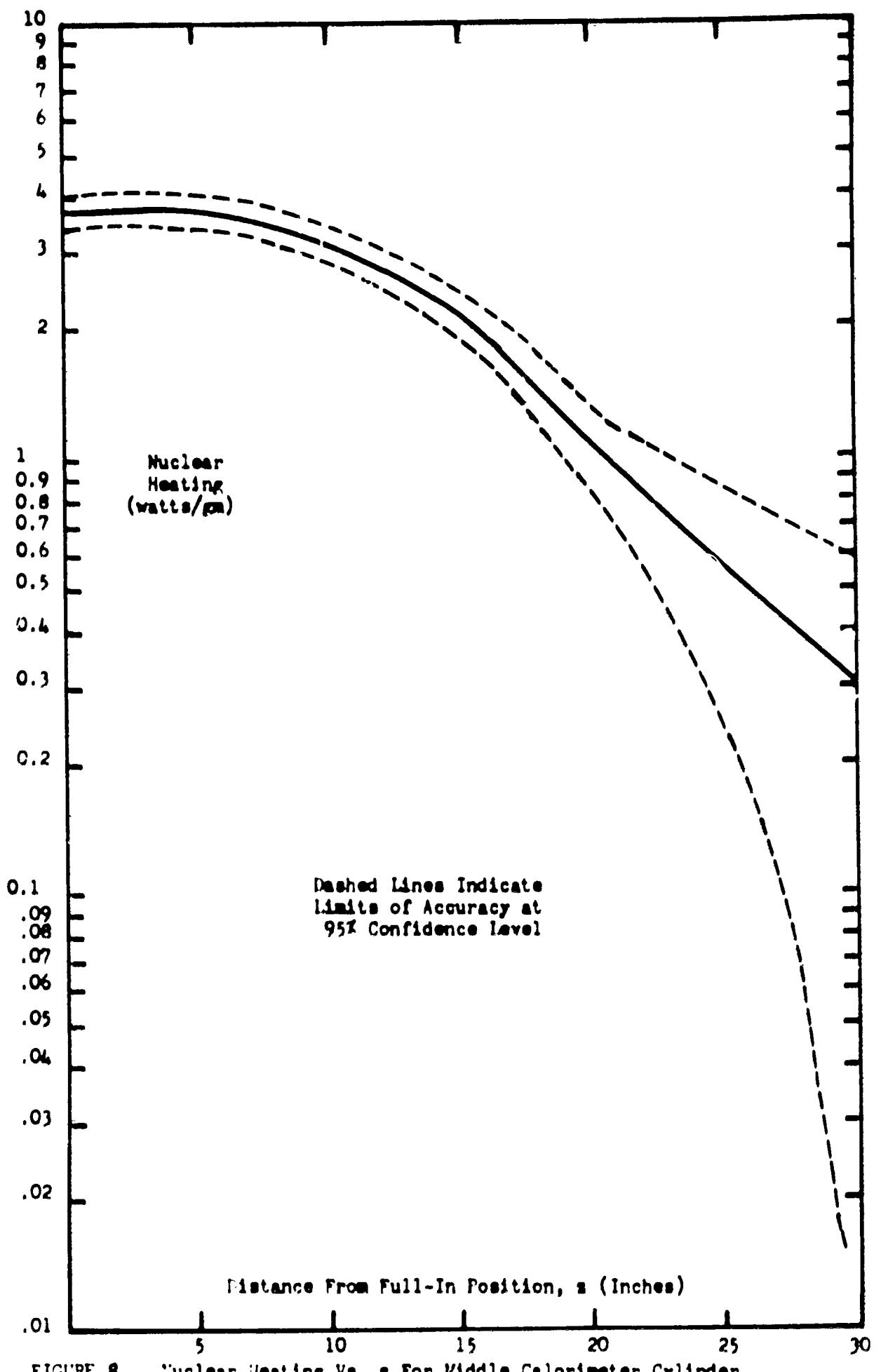


FIGURE 8 Nuclear Heating Vs.  $z$  For Middle Calorimeter Cylinder

F-8

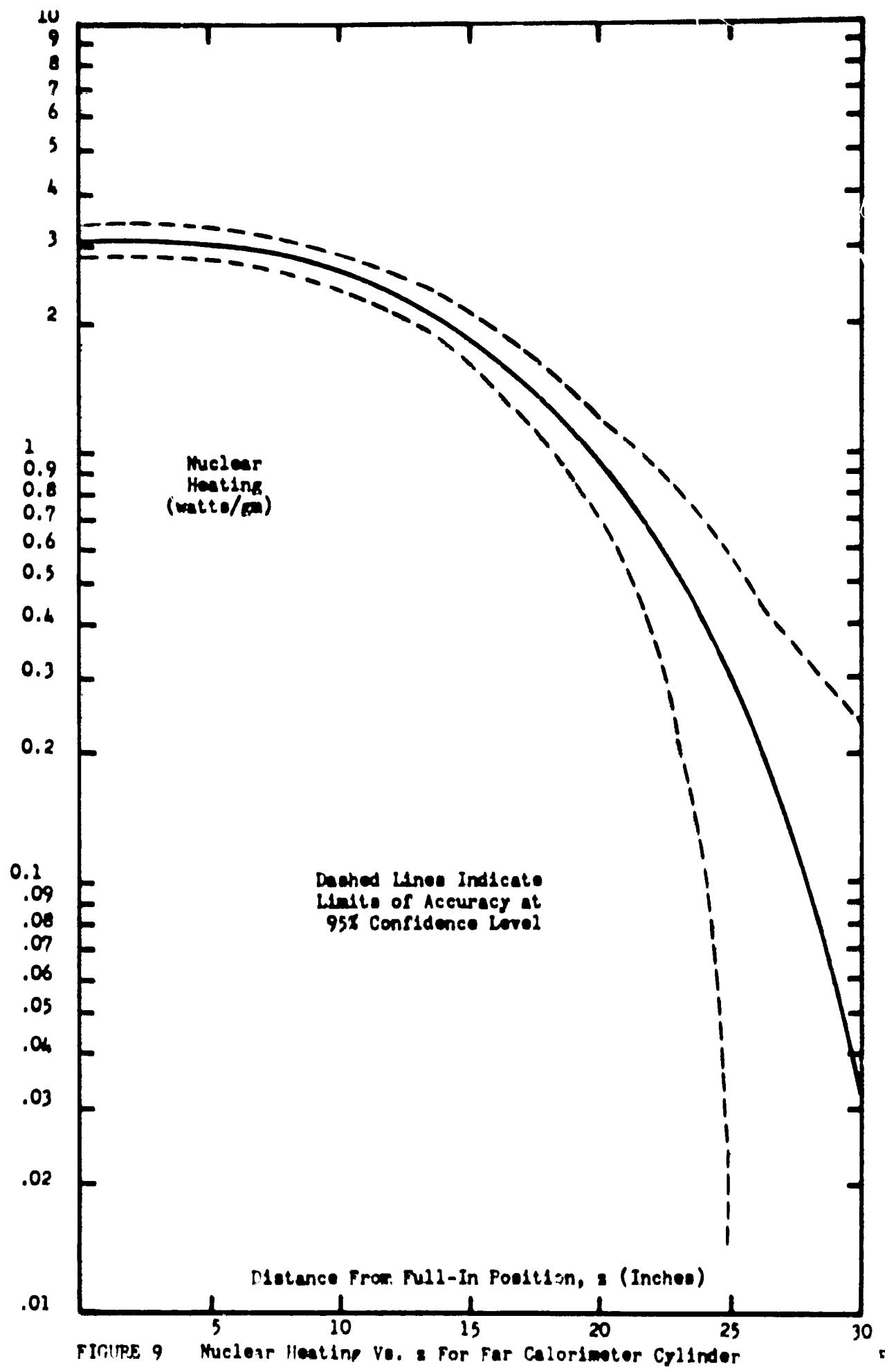


FIGURE 9 Nuclear Heating Vs. z For Far Calorimeter Cylinder

F-9

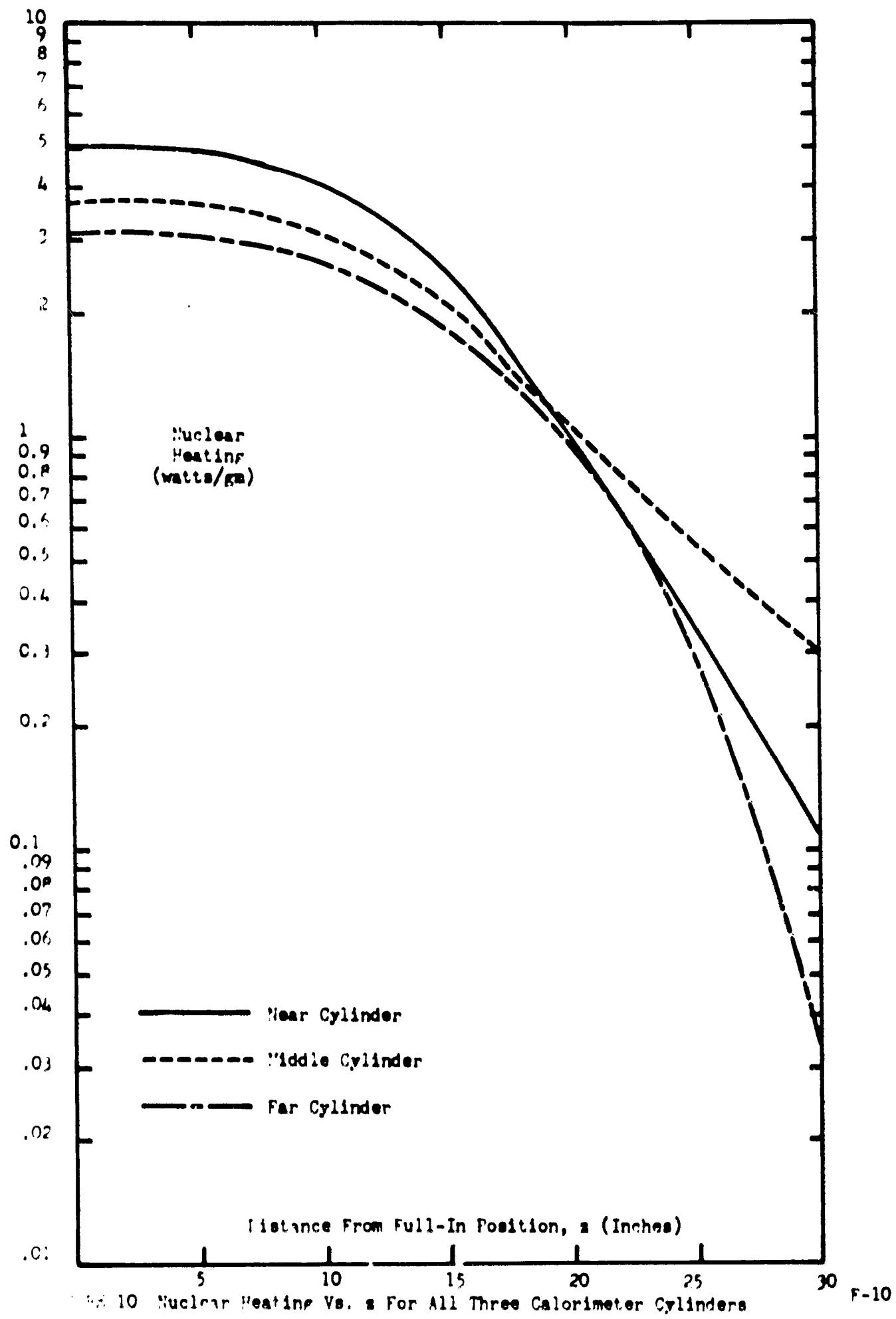


Fig. 10 Nuclear Heating Vs.  $z$  For All Three Calorimeter Cylinders

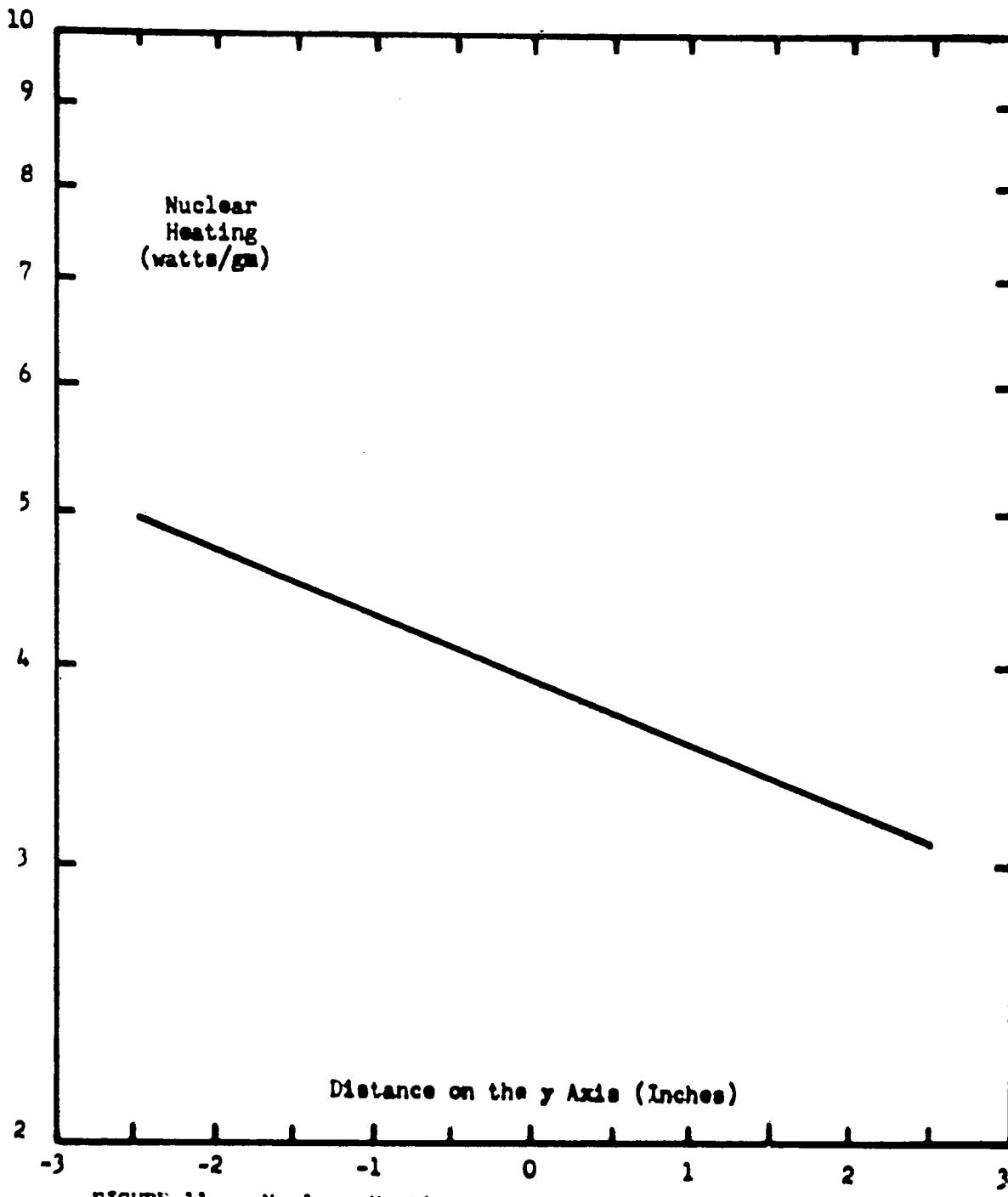


FIGURE 11 Nuclear Heating Vs.  $y$ , The Horizontal Line  
Perpendicular to  $z$

F-11

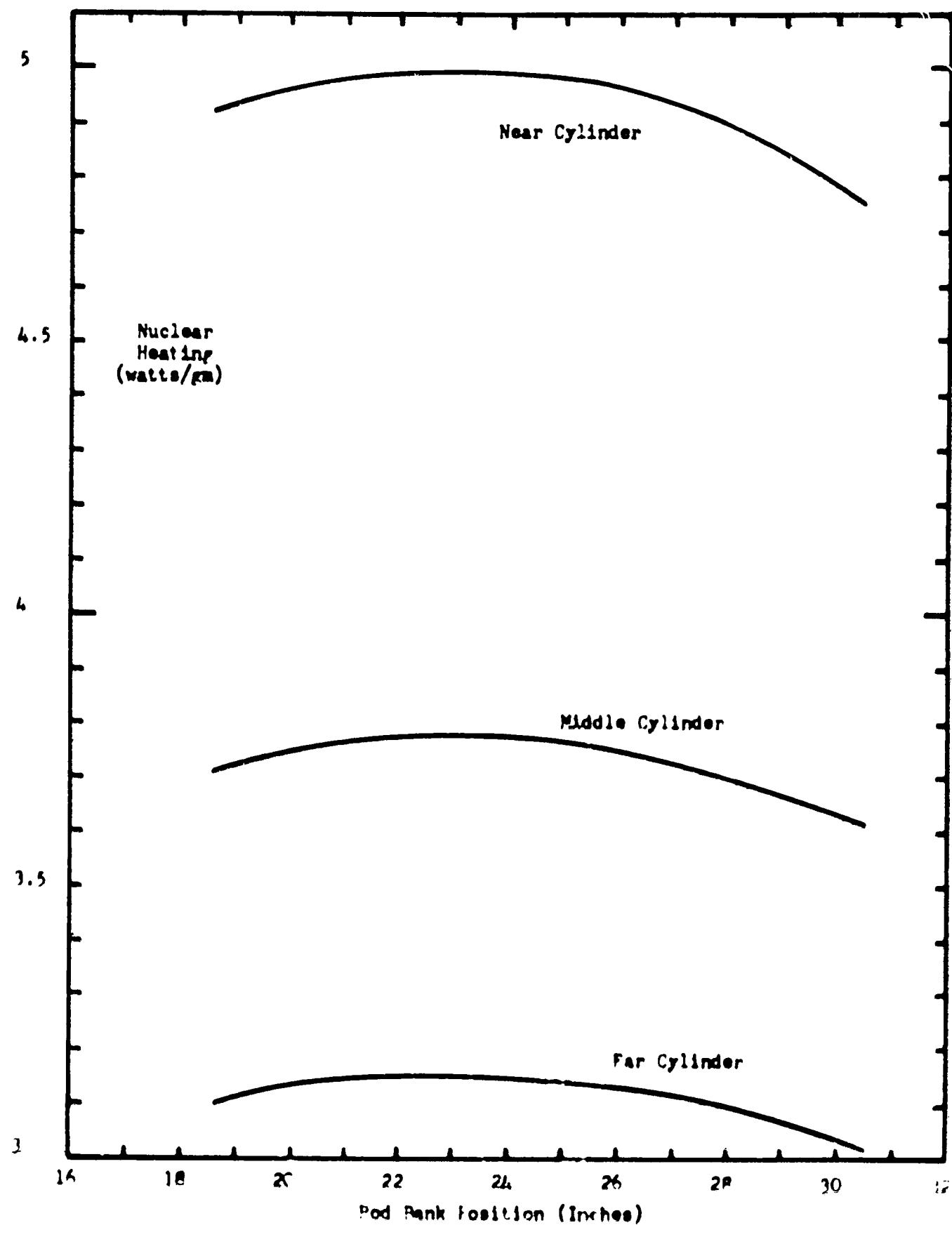


FIGURE 12 Nuclear Heating Vs. x, Pod Bank Position

F-12